

Projection Based Model Order Reduction for Multiphysical Problems

Short Course Part 2 – I | Vector Spaces and Subspace Generation

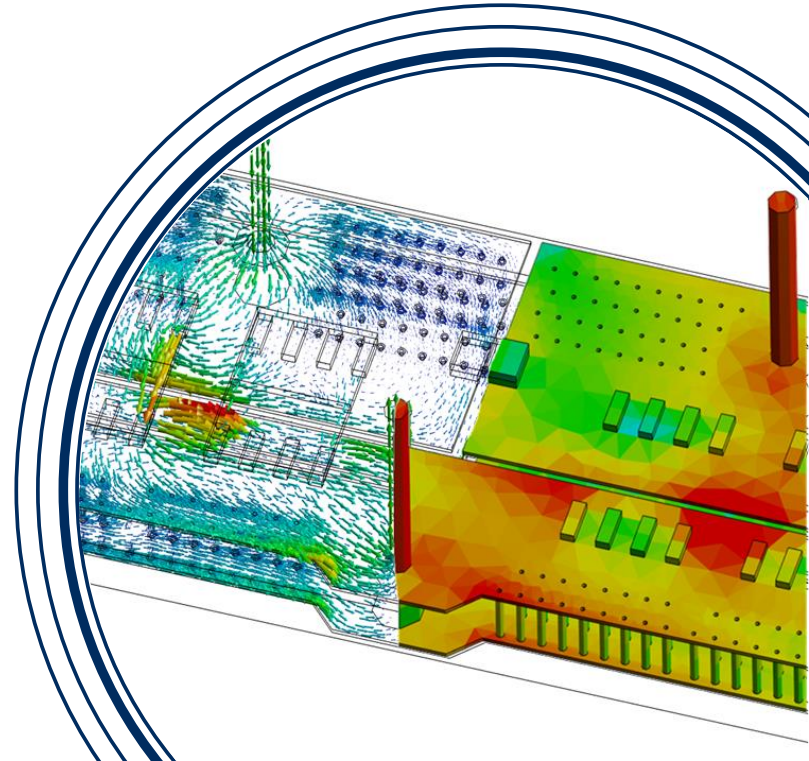
Hanna Baumgartl, Mike Feuchter, Martin Hanke

CADFEM Germany GmbH



CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



Seminarunterlagen der CADFEM Group

Das Werk einschließlich aller seiner Teile ist urheberrechtlich geschützt. Jede Verwertung außerhalb der Schranken des Urheberrechtsgesetzes ist ohne vorherige Zustimmung des Rechteinhabers unzulässig. Zur Nutzung des Werks sind ausschließlich die Personen berechtigt, die im mit dem Rechteinhaber über die Nutzung des Werks geschlossenen Vertrag namentlich definiert sind. Diese Nutzer haben ein einfaches, nicht übertragbares Recht, zeitlich befristet das Werk ausschließlich zum Zwecke der persönlichen Fortbildung zu nutzen. Jede weitergehende Nutzung, insbesondere die Weitergabe des Werks oder von Teilen davon (z.B. von Screenshots) an Dritte, einschließlich Kollegen, bedarf der vorherigen Zustimmung des Rechteinhabers.

Training Documents of CADFEM Group

The work including all its parts is protected by copyright. Any exploitation beyond the limits of the copyright law is not permitted without the prior consent of the copyright holder. Only those persons are entitled to use the work who are defined by name in the contract concluded with the rights holder concerning the use of the work. These users have a simple, non-transferable right to use the work for a limited period of time exclusively for the purpose of personal training. Any further use, in particular the transfer of the work or parts thereof (e.g. screenshots) to third parties, including colleagues, requires the prior consent of the copyright holder.

Image & Video Rights

Cover and intermediate slides: Adobe Stock

Unless otherwise stated, the image and video rights in this presentation are held by CADFEM Group.

Discrete Fourier Transformation

...is some kind of model order reduction

CADFEM / Ansys / APEX CHANNEL PARTNER

Discrete Fourier Transformation and Vector Space

CADFEM / Ansys / APEX CHANNEL PARTNER

Vector Space

CADFEM / Ansys / APEX CHANNEL PARTNER

Link to Model Order Reduction

PCB Model

CADFEM / Ansys / APEX CHANNEL PARTNER

How to find a good Subspace

Modal Analysis
 Krylov Subspace - Implicit Moment Matching

CADFEM

How to find a good Subspace

Based on Simulation Results
 Gram Schmidt Orthogonalization
 Proper Orthogonal Decomposition

- FULL
 - Taylor
 s

CADFEM / Ansys / APEX CHANNEL PARTNER

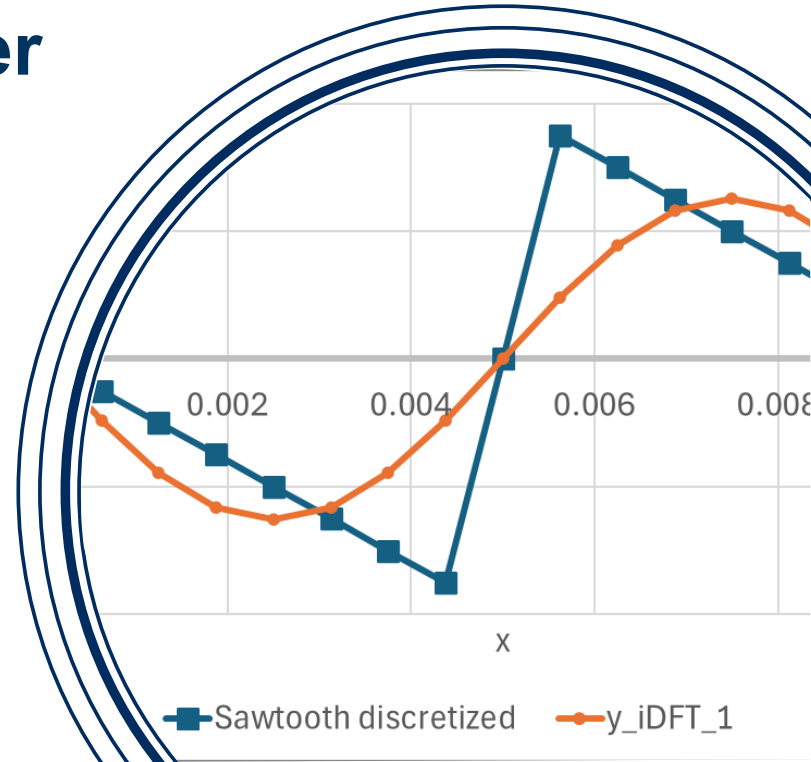
Discrete Fourier Transformation

...is some kind of model order reduction



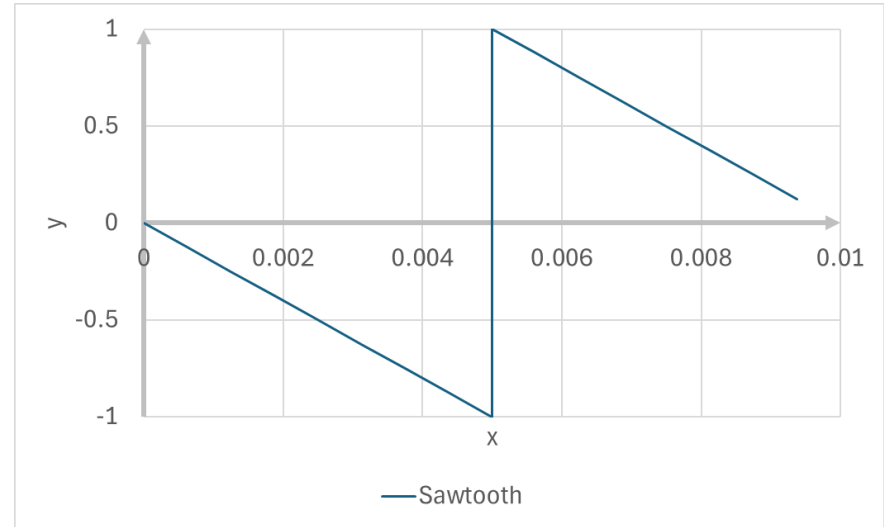
CADFEM®

Ansys / APEX CHANNEL PARTNER



Starting point

- Continuous series $y(x) \in \mathbb{R}^\infty$
→ Infinite number of points



Discrete Fourier Transformation



Discretization

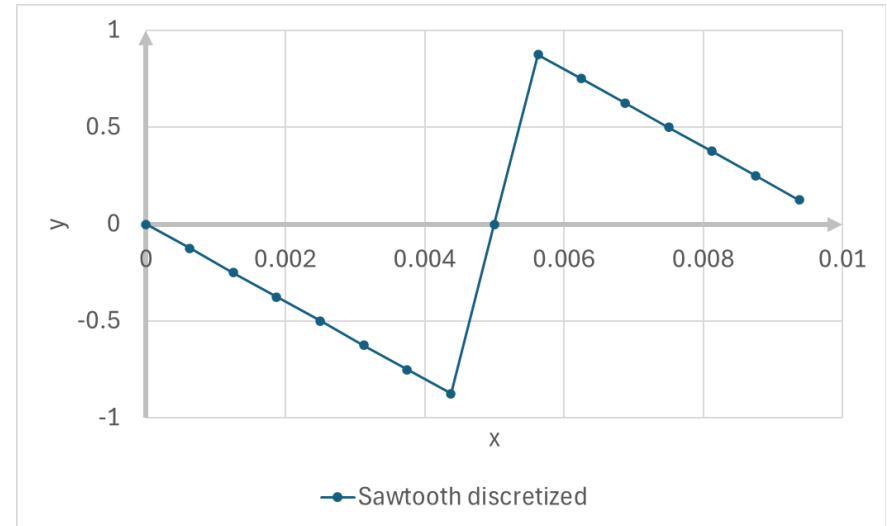
Starting point

- Continuous series $y(x) \in \mathbb{R}^\infty$
→ Infinite number of points

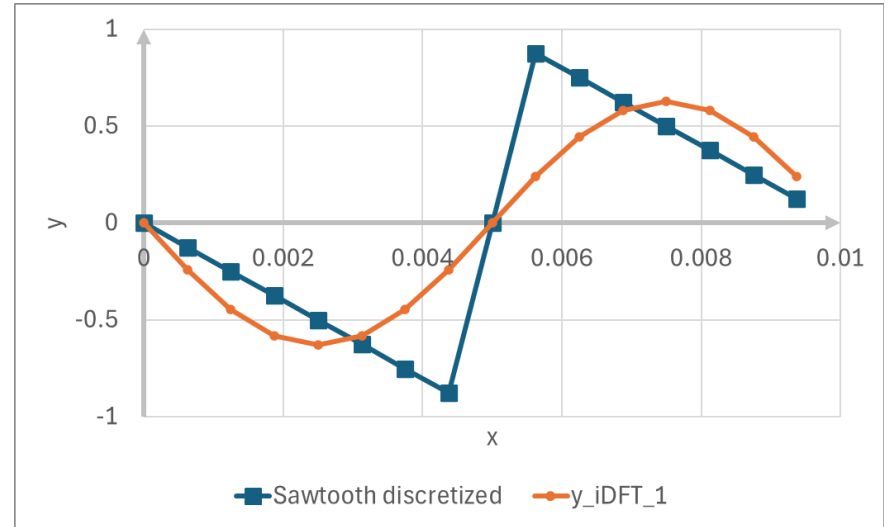
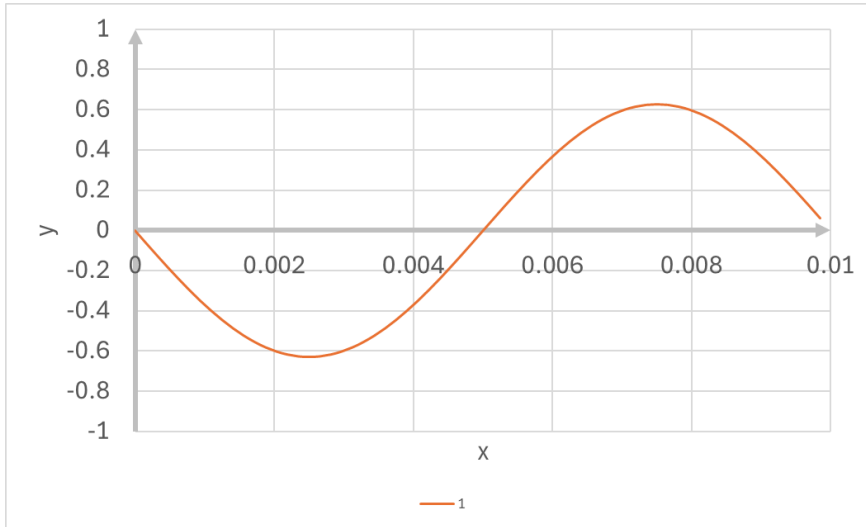
Discretized

- $\mathbf{y} = \{y_0, \dots, y_{N-1}\} \mathbf{y} \in \mathbb{R}^N$
- N Number of timepoints

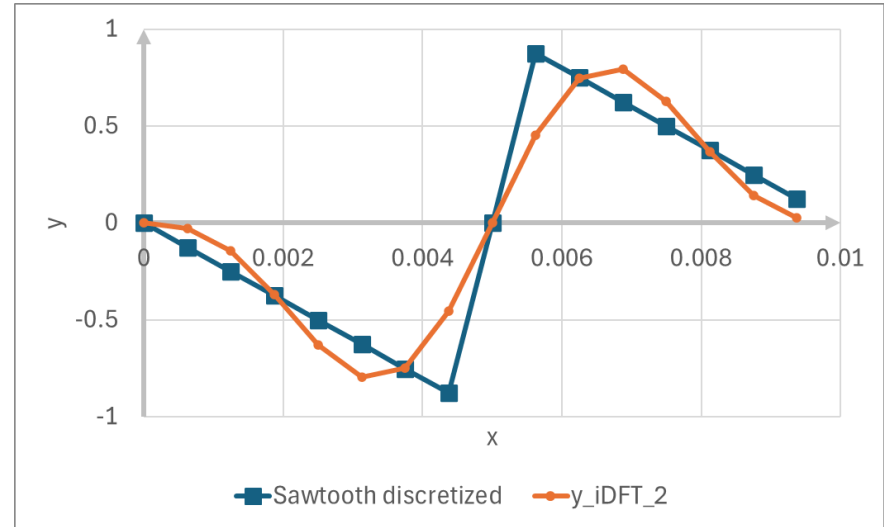
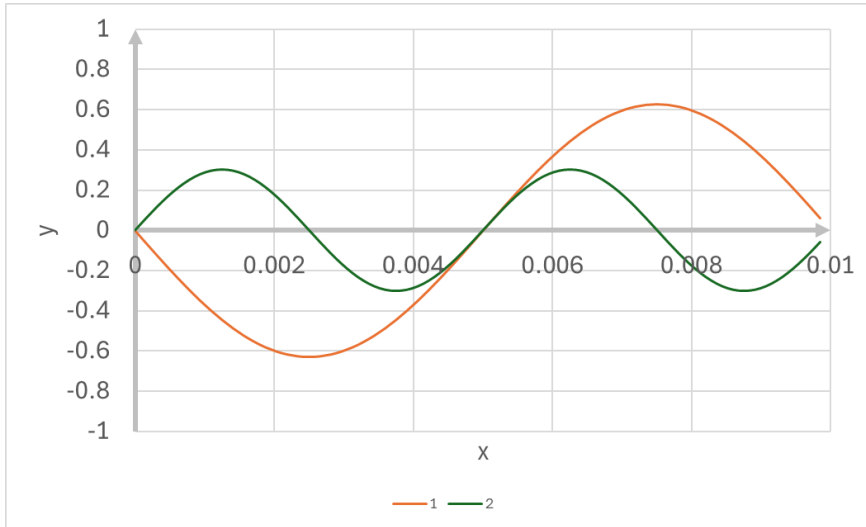
→ From infinite to N 😊



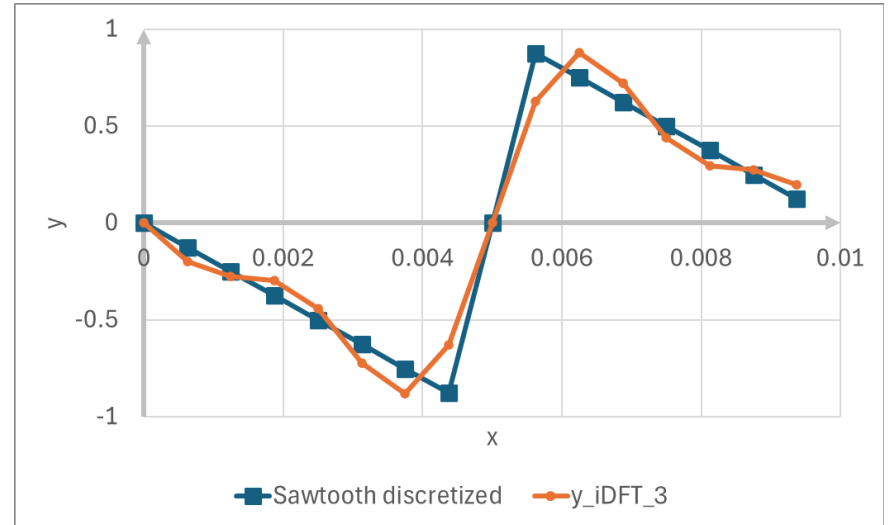
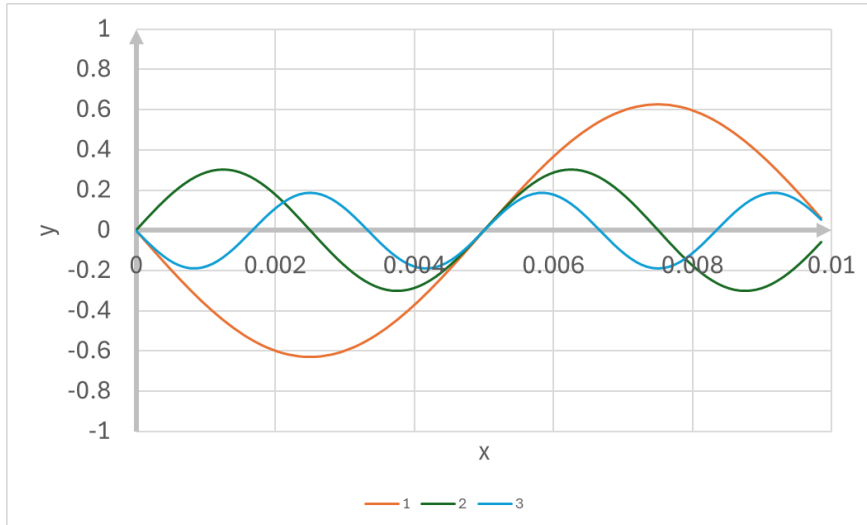
Discrete Fourier Transformation



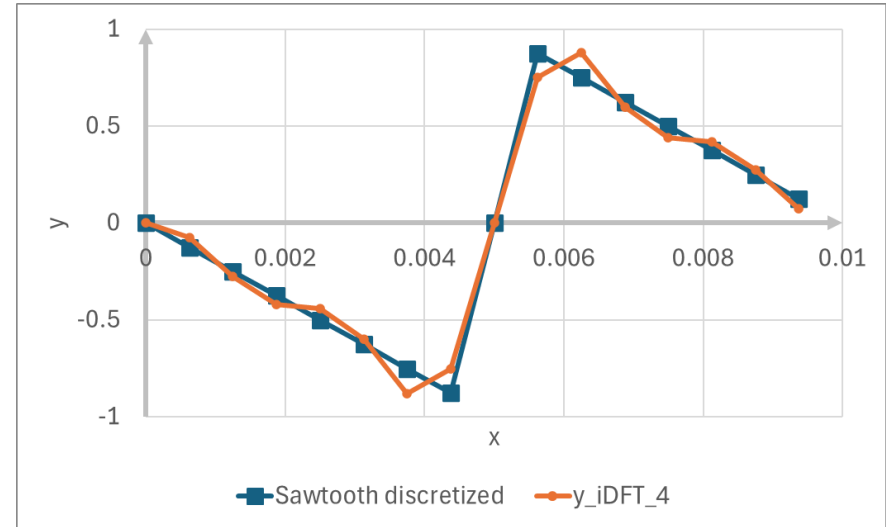
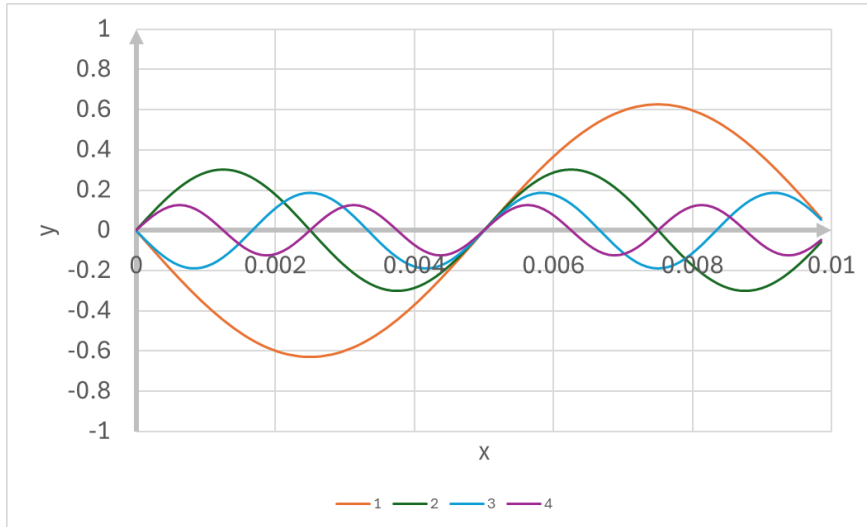
Discrete Fourier Transformation



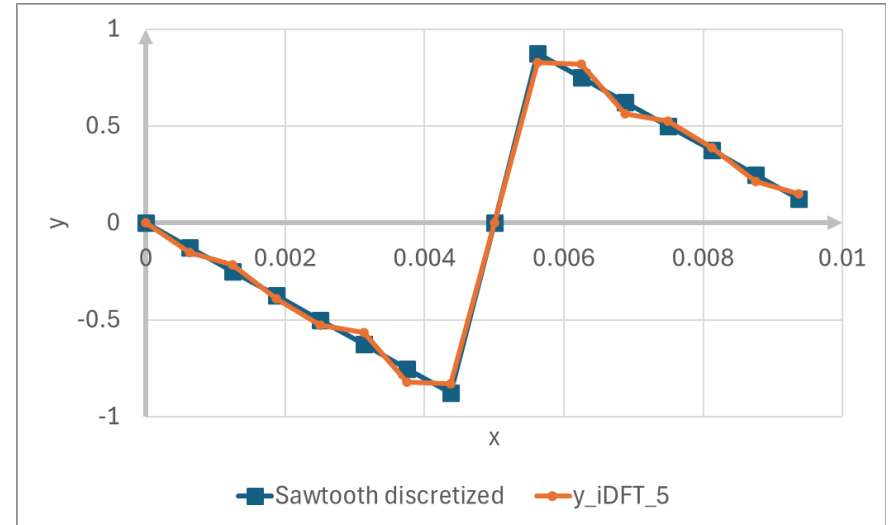
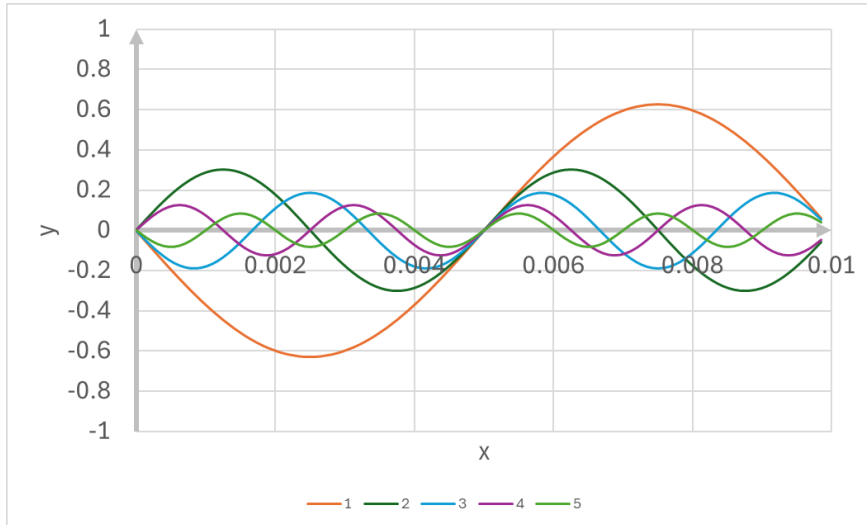
Discrete Fourier Transformation



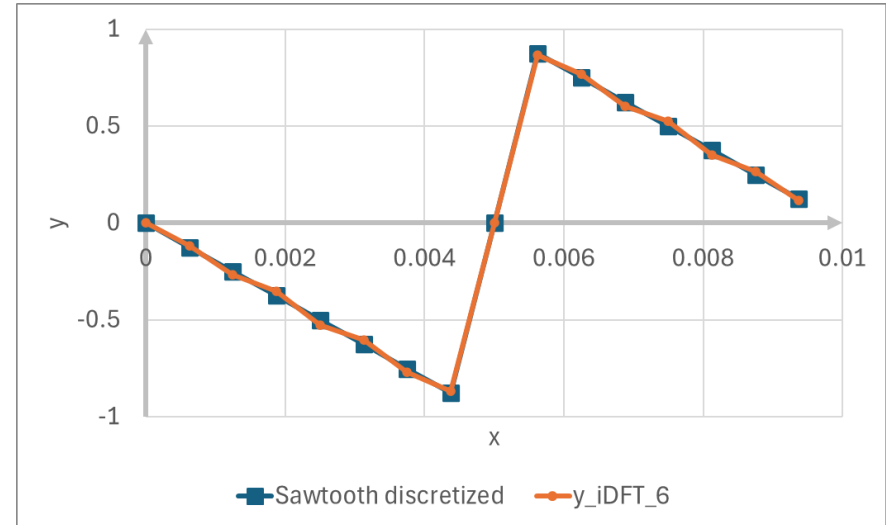
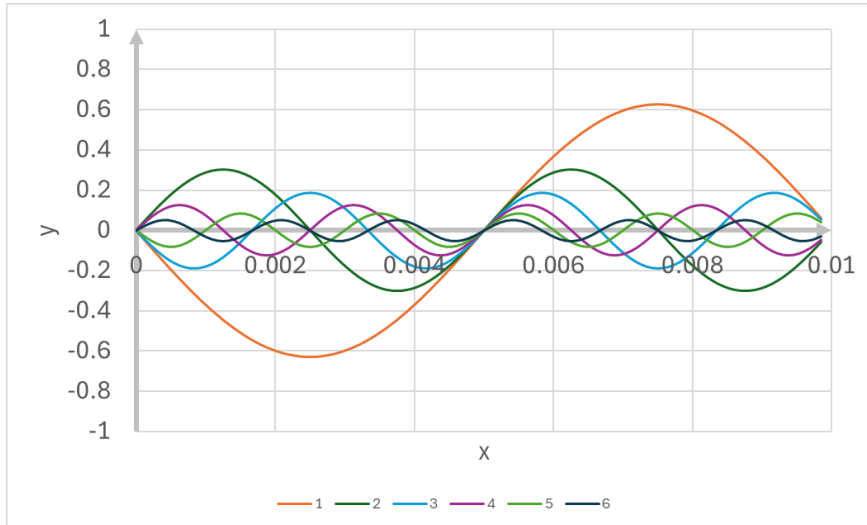
Discrete Fourier Transformation



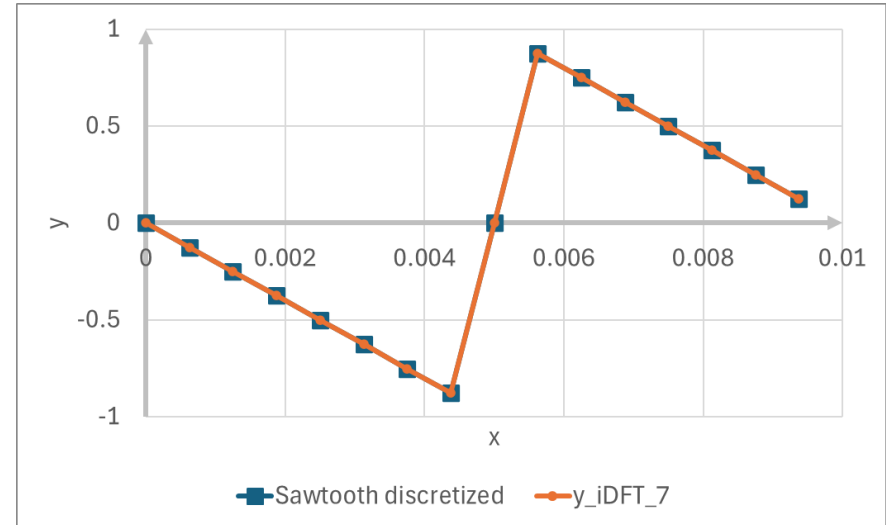
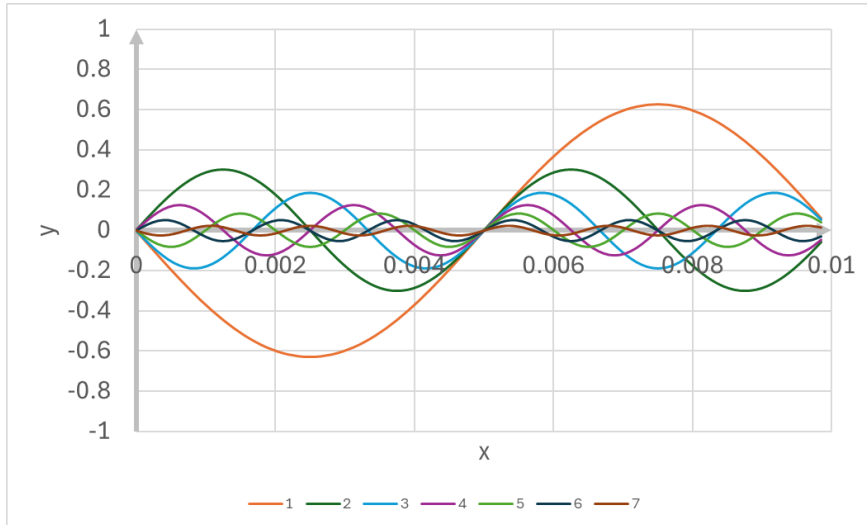
Discrete Fourier Transformation



Discrete Fourier Transformation



Discrete Fourier Transformation

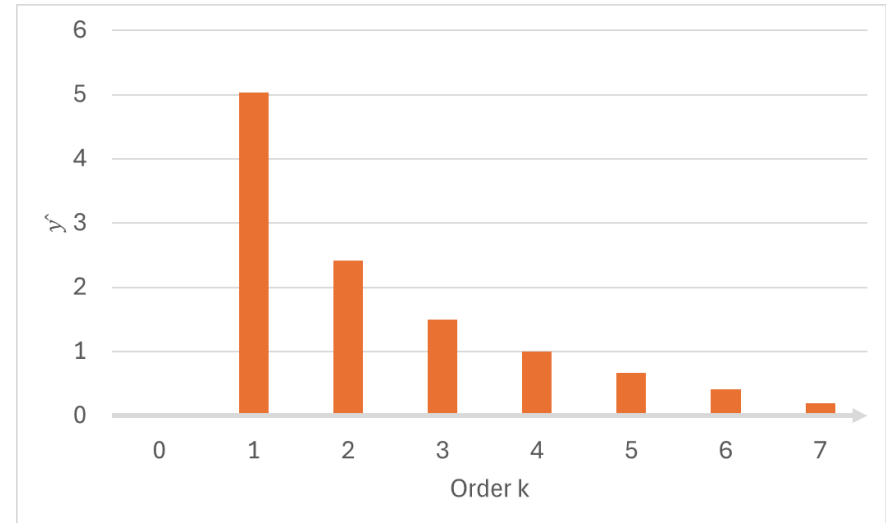


Fourier Coefficients

- $\hat{y}_k = \sum_{j=0}^{N-1} e^{-2\pi i \frac{jk}{N}} y_j$
- for $k = 0, \dots, N - 1$

In Matrix Notation

- $\hat{\mathbf{y}} = \mathbf{\Phi}^T \mathbf{y}$
- with $\mathbf{\Phi}[j, k] = e^{-2\pi i \frac{jk}{N}}$

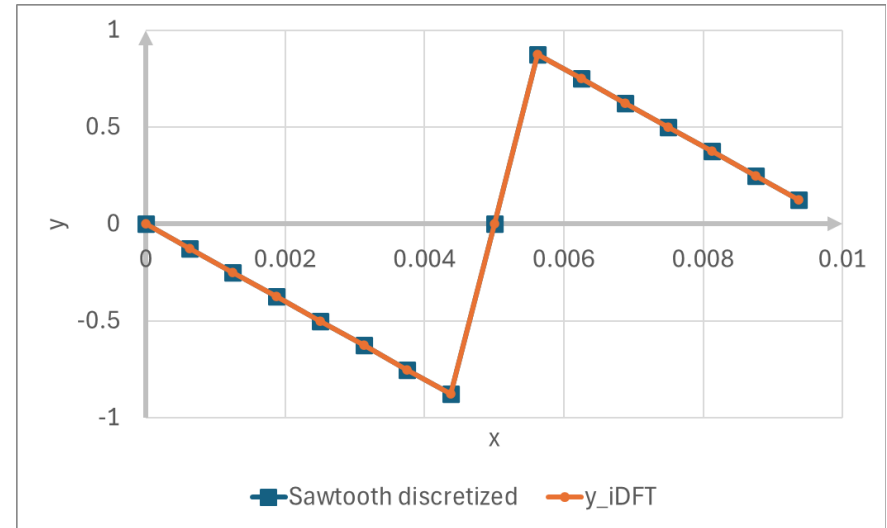


Inverse Discrete Fourier Transformation

- $y_k = \frac{1}{N} \sum_{j=0}^{N-1} e^{2\pi i \frac{jk}{N}} \hat{y}_j$
- for $k = 0, \dots, N - 1$

In Matrix Notation

- $\mathbf{y} = [\Phi^T]^{-1} \hat{\mathbf{y}}$
- with $\Phi[j, k] = e^{-2\pi i \frac{jk}{N}}$



Discrete Fourier Transformation



Link to model order reduction?

Discretized signal

- $y = \{y_0, \dots, y_{N-1}\} y \in \mathbb{R}^N$, Order N

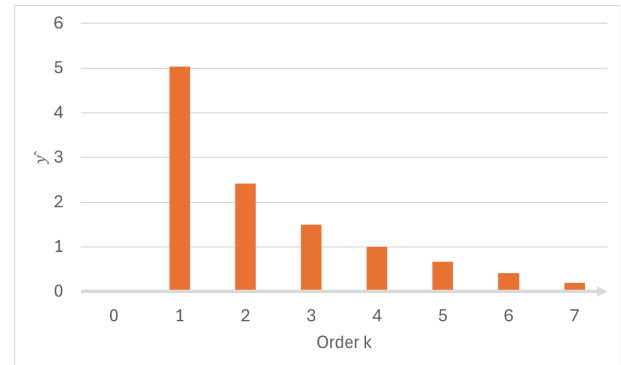
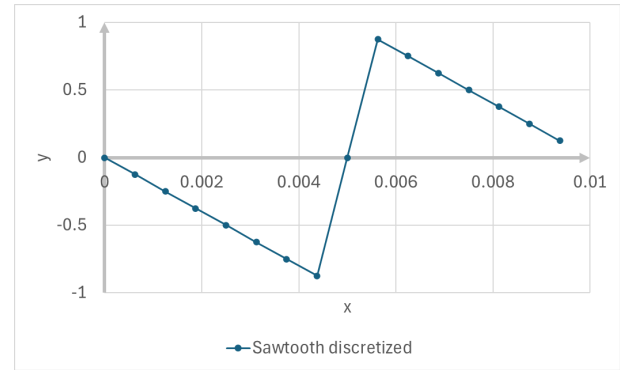
Representation by DFT

- $\hat{y}_k = \sum_{j=0}^{N-1} e^{-2\pi i \frac{jk}{N}} y_j$, $\hat{y} \in \mathbb{R}^N$, Order N
- for $k = 0, \dots, N - 1$

The same data is represented

- ...but in different coordinates
- They can be interpreted in a different way

Let's call \hat{y} generalized coordinates



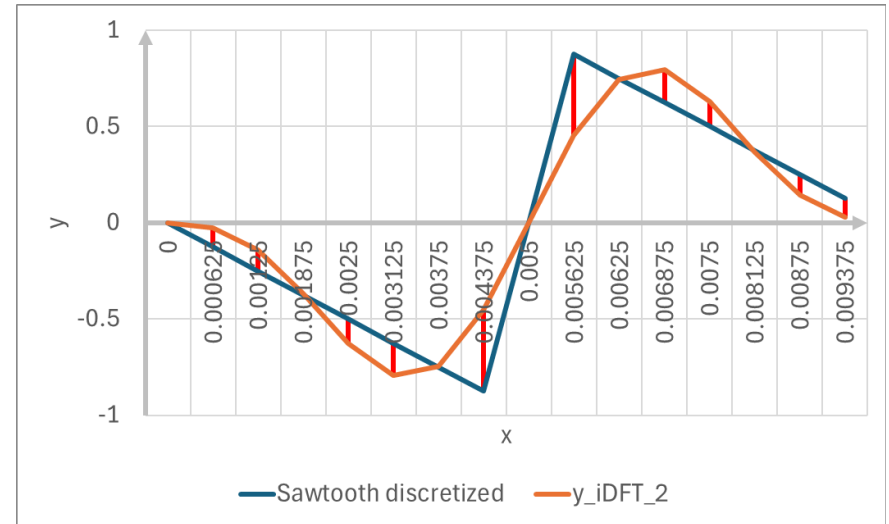
Discrete Fourier Transformation

...is some kind of model order reduction



Reduce Dimension

- By taking less Fourier coefficients
- Error is introduced

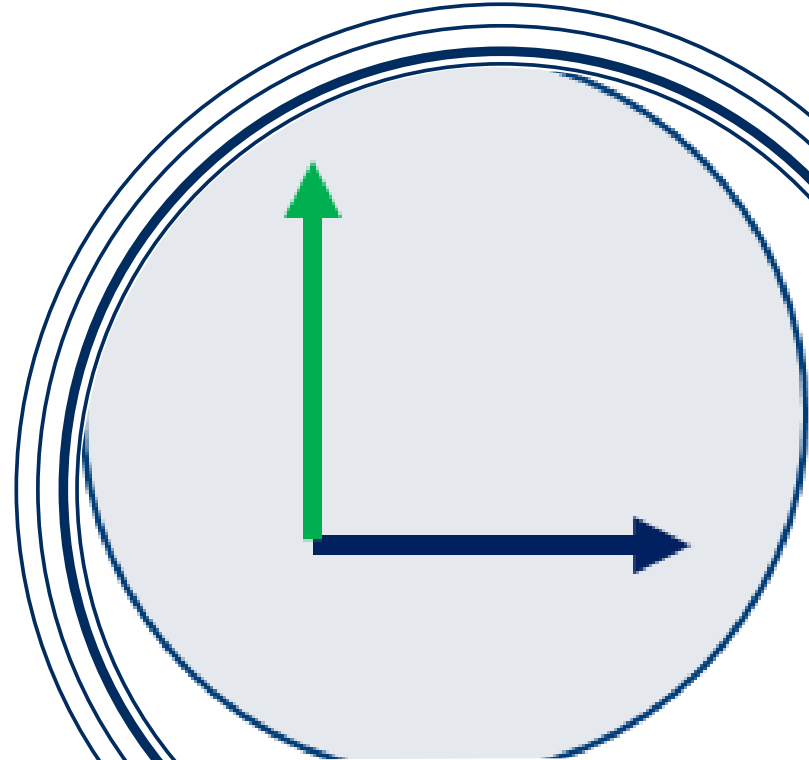


Vector Space



CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



Vector Space V



Vector **a**

Mechanical
engineer

- Force

CFD

- Velocity

Electrical
engineer

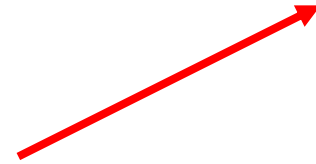
- Voltage in the
complex plane

My girlfriend

- There is nothing this
arrow points on

Mathematician

- A vector in \mathbb{R}^2



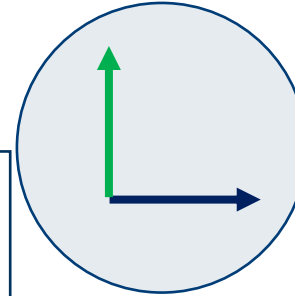
Vector Space V



Basis of Vector Space

Basis B

- ...of a vector space V with basis vectors \mathbf{b}_1 to \mathbf{b}_m
- $\mathbf{B} = [\mathbf{b}_1, \dots, \mathbf{b}_m] \in \mathbb{R}^m$
- m is the dimension of the vector space



Those basis vectors must be linear independent

- Each vector can be represented as a linear combination of basis vectors and this representation is unique
- Euclidian basis \mathbb{R}^m (also called standard, natural or canonical basis)
 - $\mathbf{b}_1 = \begin{Bmatrix} 1 \\ 0 \end{Bmatrix}$, $\mathbf{b}_2 = \begin{Bmatrix} 0 \\ 1 \end{Bmatrix}$
 - $\mathbf{B}_1 = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} = \mathbf{I}$

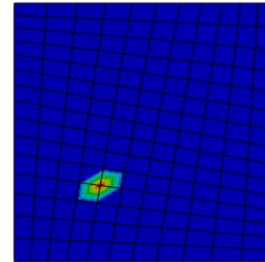
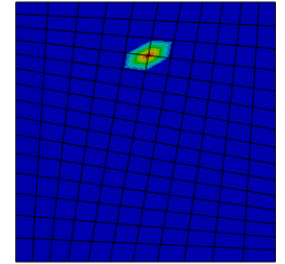
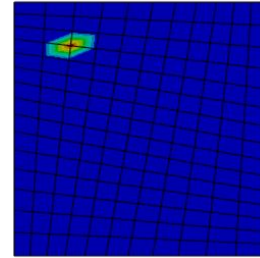
Vector Space V

Basis of Vector Space



FEM

- “1” at one node, all others are 0
- $\in \mathbb{R}^N$
- N is the number of dofs



...

Vector Space V



Coordinates of a vector

Vector \mathbf{a}

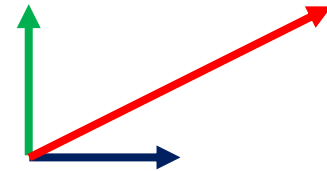
- ...with its coordinates a_1 to a_N with respect to basis \mathbf{B}_1
- $\mathbf{a} = \{a_1, \dots, a_N\} \in \mathbb{R}^N$
- E.g. $\mathbf{a} = \begin{Bmatrix} 2 \\ 1 \end{Bmatrix}$
- $2 \begin{Bmatrix} 1 \\ 0 \end{Bmatrix} + 1 \begin{Bmatrix} 0 \\ 1 \end{Bmatrix} = \mathbf{B}_1 \mathbf{a} = \begin{Bmatrix} 2 \\ 1 \end{Bmatrix}$

Each vector can be represented

- ...as a linear combination of basis vectors
- and this representation is unique

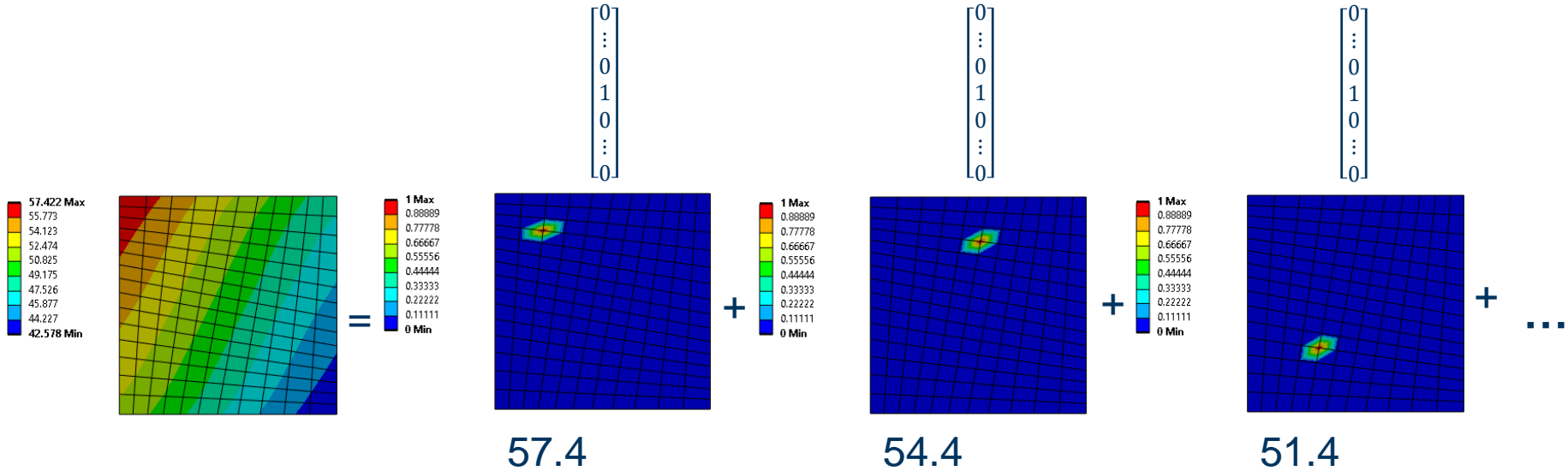
In reduced order modeling

- $\mathbf{B}\mathbf{a}$ is called Expansion



Vector Space V

Coordinates of a vector



Vector Space V



The basis is not unique!

Different basis

• E.g. $\mathbf{b}_3 = \begin{Bmatrix} \frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} \end{Bmatrix}$, $\mathbf{b}_4 = \begin{Bmatrix} -\frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} \end{Bmatrix}$

• $\mathbf{B}_2 = \begin{bmatrix} \frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{bmatrix}$

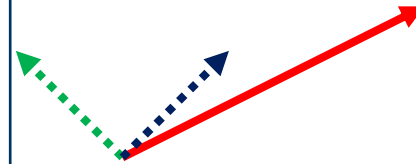
• spans the same vector space

Vector \mathbf{a}

• ...with its coordinates $\hat{\mathbf{a}}_1$ to $\hat{\mathbf{a}}_N$ with respect to basis \mathbf{B}_2

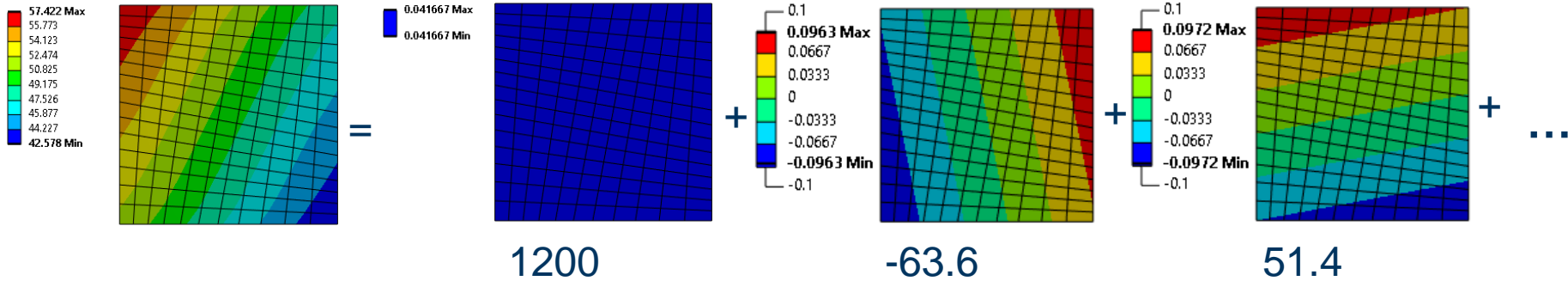
• $\hat{\mathbf{a}} = \begin{Bmatrix} 2.12 \\ -0.71 \end{Bmatrix}$

• $2.12 \begin{Bmatrix} \frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} \end{Bmatrix} + -0.71 \begin{Bmatrix} -\frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} \end{Bmatrix} = \mathbf{B}_2 \hat{\mathbf{a}}$



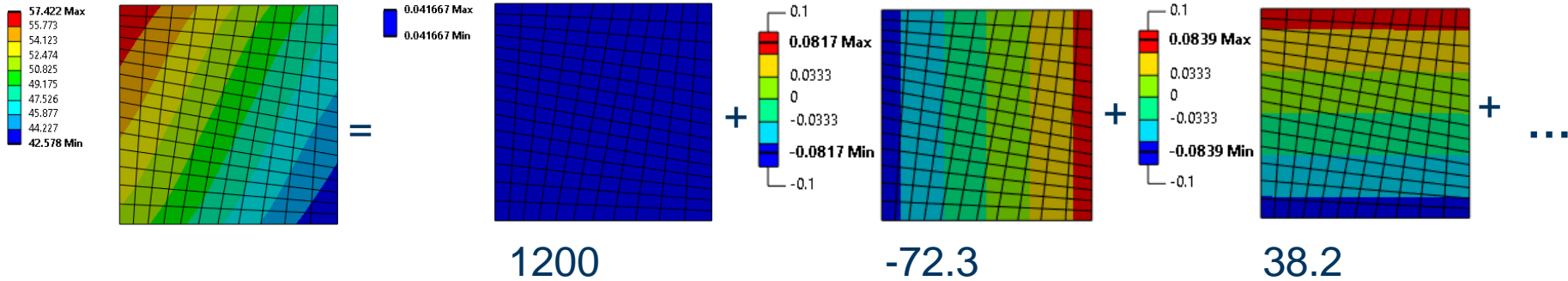
Vector Space V

The basis is not unique!



Vector Space V

The basis is not unique!



Vector Space V

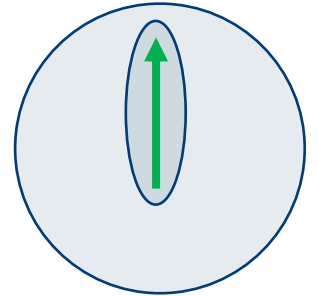
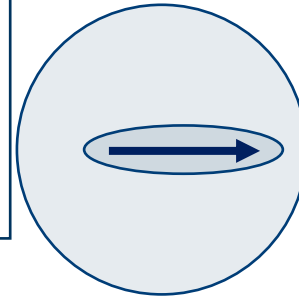
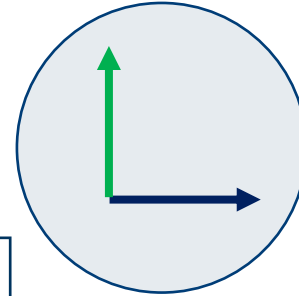


Truncated Basis

One can truncate the basis by neglecting some basis vectors

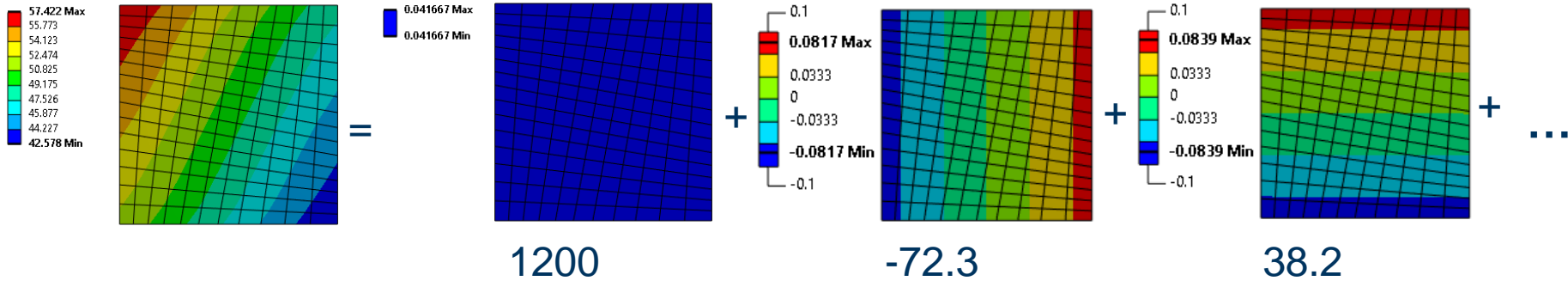
- $B_1 = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$
- E.g. $B_{1_1} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$ or $B_{1_2} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$

The truncated basis spans a subspace of V



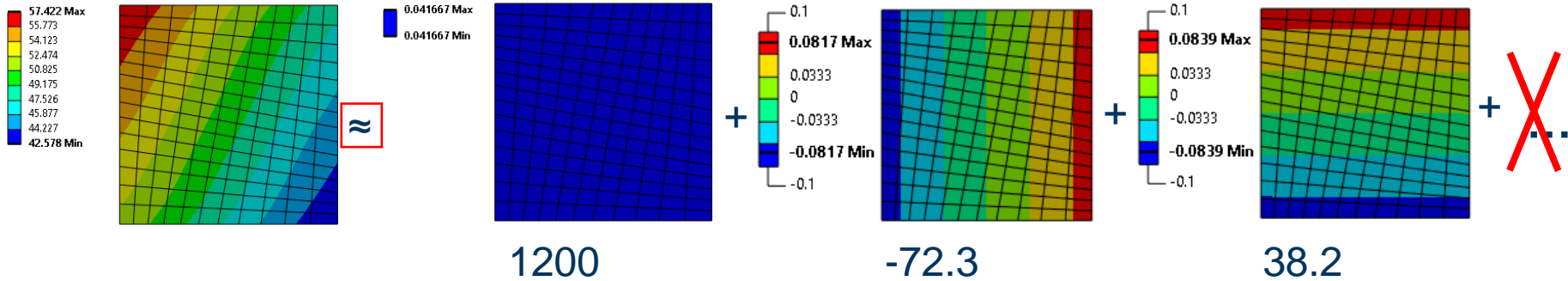
Vector Space V

Truncated Basis



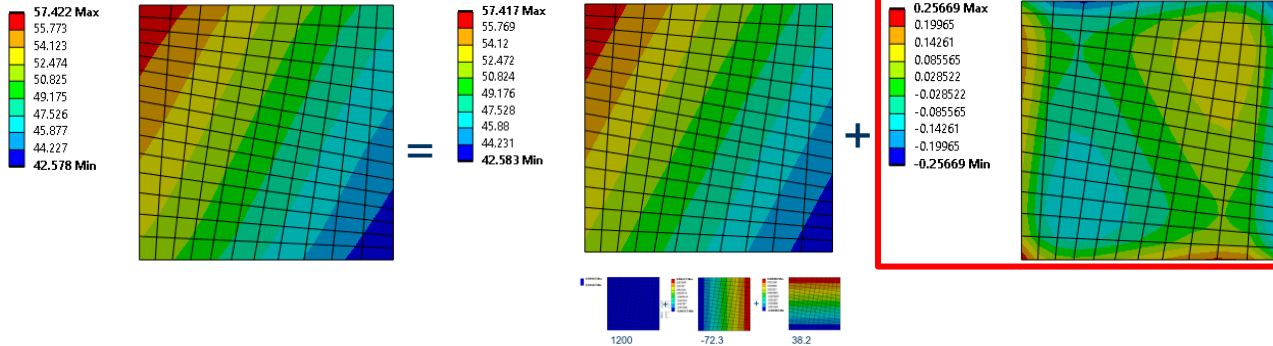
Vector Space V

Truncated Basis



Vector Space V

Truncated Basis



Scalar Product

- Mathematical relationship that assigns a scalar to two vectors
- Often denoted as by $\langle \mathbf{a}, \mathbf{c} \rangle$
- $\langle \mathbf{a}, \mathbf{c} \rangle = \mathbf{a}^T \mathbf{c} = \sum_{j=1}^N a_j c_j = a_1 c_1 + \dots + a_N c_N$
- E.g. $\mathbf{a} = \begin{Bmatrix} 2 \\ 1 \end{Bmatrix}$, $\mathbf{c} = \begin{Bmatrix} 0 \\ 1 \end{Bmatrix}$
- $\mathbf{a}^T \mathbf{c} = 2 \cdot 0 + 1 \cdot 1 = 1$



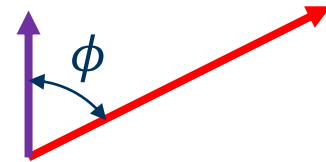
Vector Space V

Scalar product / Inner Product



Geometric interpretation in \mathbb{R}^2

- $\mathbf{a}^T \mathbf{c} = \|\mathbf{a}\| \|\mathbf{c}\| \cos(\phi)$
- $\phi = \arccos\left(\frac{\mathbf{a}^T \mathbf{c}}{\|\mathbf{a}\| \|\mathbf{c}\|}\right)$
- E.g. $\mathbf{a} = \begin{Bmatrix} 2 \\ 1 \end{Bmatrix}$, $\mathbf{c} = \begin{Bmatrix} 0 \\ 1 \end{Bmatrix}$
- $\phi = \arccos\left(\frac{2 \cdot 0 + 1 \cdot 1}{\sqrt{5} \cdot 1}\right) = 63^\circ$



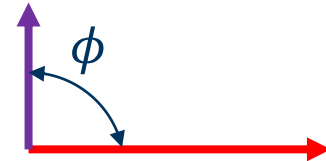
Vector Space V

Orthogonality



Two vectors are orthogonal if the scalar product is 0

- In \mathbb{R}^2 the angle is 90°
- E.g. $\mathbf{a} = \begin{Bmatrix} 2 \\ 0 \end{Bmatrix}$, $\mathbf{c} = \begin{Bmatrix} 0 \\ 1 \end{Bmatrix}$
- $\mathbf{a}^T \mathbf{c} = 2 \cdot 0 + 0 \cdot 1 = 0$



Orthogonal Basis

Orthogonal basis

- The scalar product is 0 for $\mathbf{b}_i^T \mathbf{b}_j$ with $i \neq j$

$$\mathbf{B}_1^T \mathbf{B}_1$$

$$\bullet = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 \cdot 1 + 0 \cdot 0 & 1 \cdot 0 + 0 \cdot 0 \\ 0 \cdot 1 + 1 \cdot 0 & 0 \cdot 0 + 1 \cdot 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

$$\mathbf{B}_2^T \mathbf{B}_2$$

$$\bullet = \begin{bmatrix} \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \\ \frac{-\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{bmatrix} \begin{bmatrix} \frac{\sqrt{2}}{2} & \frac{-\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{bmatrix} = \begin{bmatrix} \frac{\sqrt{2}}{2} \cdot \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2} \cdot \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \cdot \frac{-\sqrt{2}}{2} + \frac{\sqrt{2}}{2} \cdot \frac{\sqrt{2}}{2} \\ \frac{-\sqrt{2}}{2} \cdot \frac{\sqrt{2}}{2} + \frac{\sqrt{2}}{2} \cdot \frac{\sqrt{2}}{2} & \frac{-\sqrt{2}}{2} \cdot \frac{-\sqrt{2}}{2} + \frac{\sqrt{2}}{2} \cdot \frac{\sqrt{2}}{2} \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

Vector Space V

Orthogonal Projection



Given vector \mathbf{a}

$$\bullet \mathbf{a} = \begin{Bmatrix} 2 \\ 1 \end{Bmatrix}$$

w.r.t to basis \mathbf{B}_1

$$\bullet \mathbf{B}_1 = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

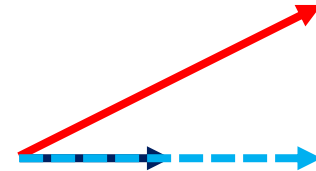
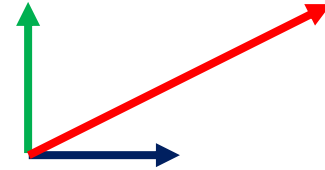
$$\bullet \mathbf{B}_1 \mathbf{a} = 2 \begin{Bmatrix} 1 \\ 0 \end{Bmatrix} + 1 \begin{Bmatrix} 0 \\ 1 \end{Bmatrix}$$

Projection onto truncated basis $\mathbf{B}_{1_1} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$

$$\bullet \hat{\mathbf{a}}_1 = \mathbf{B}_{1_1}^T \mathbf{a} = [1 \quad 0] \begin{Bmatrix} 2 \\ 1 \end{Bmatrix} = 2$$

Projection onto truncated basis $\mathbf{B}_{1_2} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$

$$\bullet \hat{\mathbf{a}}_2 = \mathbf{B}_{1_2}^T \mathbf{a} = [0 \quad 1] \begin{Bmatrix} 2 \\ 1 \end{Bmatrix} = 1$$



Vector Space V

Change of Basis



Change of basis of vector \mathbf{a}

- $\mathbf{a} = \begin{Bmatrix} 2 \\ 1 \end{Bmatrix}$

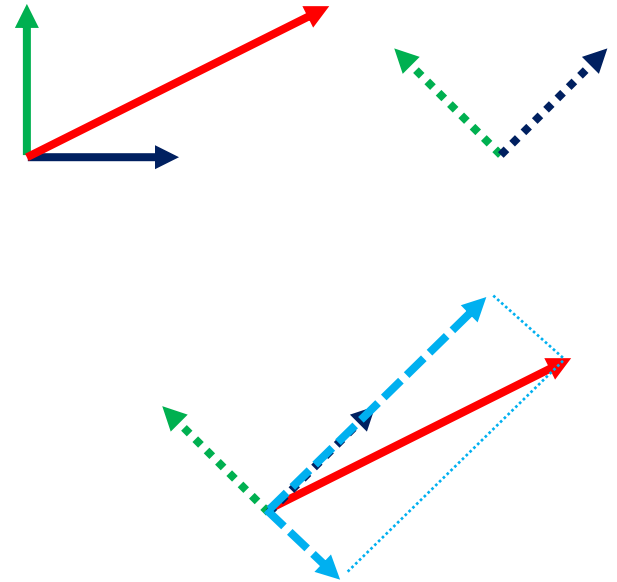
- From $\mathbf{B}_1 = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$ to $\mathbf{B}_2 = \begin{bmatrix} \frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{bmatrix}$

Linear system of equations

- $\mathbf{B}_1 \mathbf{a} = \mathbf{B}_2 \hat{\mathbf{a}}$

Solution

- $\hat{\mathbf{a}} = \mathbf{B}_2^{-1} \mathbf{B}_1 \mathbf{a}$



Vector Space V



Change of Basis - Why are orthogonal bases that nice?

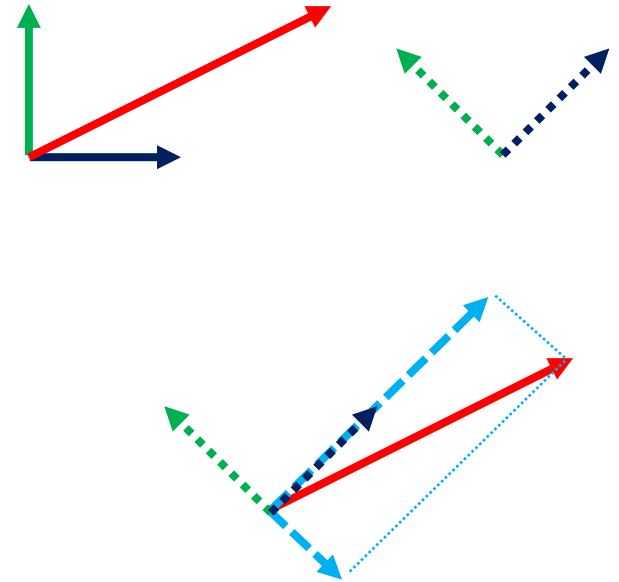
Solution

- $\hat{\mathbf{a}} = \mathbf{B}_2^{-1} \mathbf{B}_1 \mathbf{a}$

Why are orthogonal bases that nice?

- $\mathbf{B}_2^{-1} = \mathbf{B}_2^T$
- $\hat{\mathbf{a}} = \mathbf{B}_2^T \mathbf{B}_1 \mathbf{a}$

- $\hat{\mathbf{a}} = \begin{bmatrix} \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \\ -\frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{Bmatrix} 2 \\ 1 \end{Bmatrix} = \begin{Bmatrix} 2.12 \\ -.71 \end{Bmatrix}$



Vector Space V

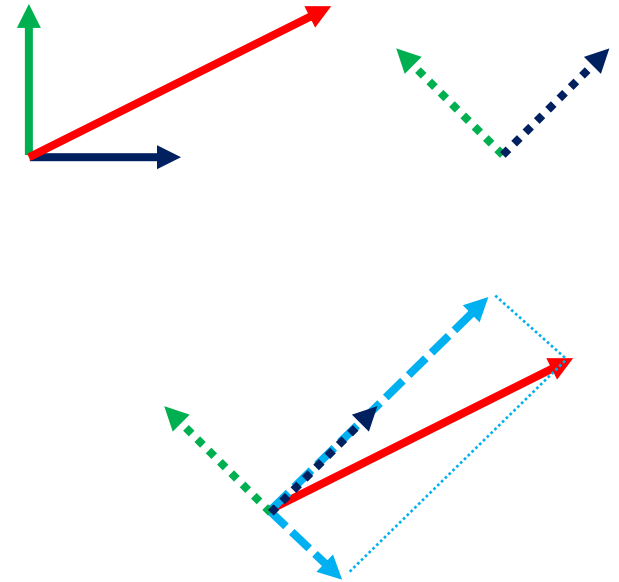
Change of Basis - Projection



$$\hat{\mathbf{a}} = \mathbf{B}_2^T \mathbf{B}_1 \mathbf{a}$$

In reduced order modeling

- If not denoted differently, the basis \mathbf{B}_1 is the Euclidian basis
- $\hat{\mathbf{a}} = \Phi^T \mathbf{a}$ is just called Projection
- The truncated basis is written as Φ , describing the subspace
- $\hat{\mathbf{a}}$ are called generalized coordinates



Vector Space V



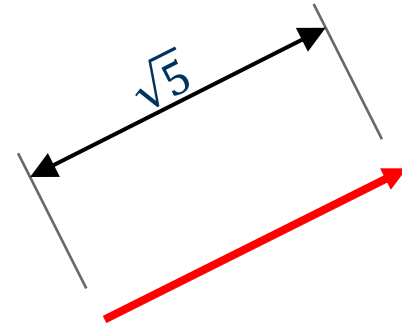
Norm

Norm

- Assigns a non-negative real number to an element of the vector space
- Often denoted as $\|\cdot\|$.
- Generalization of the intuitive notion of "length" in the physical world

Often the norm is defined by the scalar product

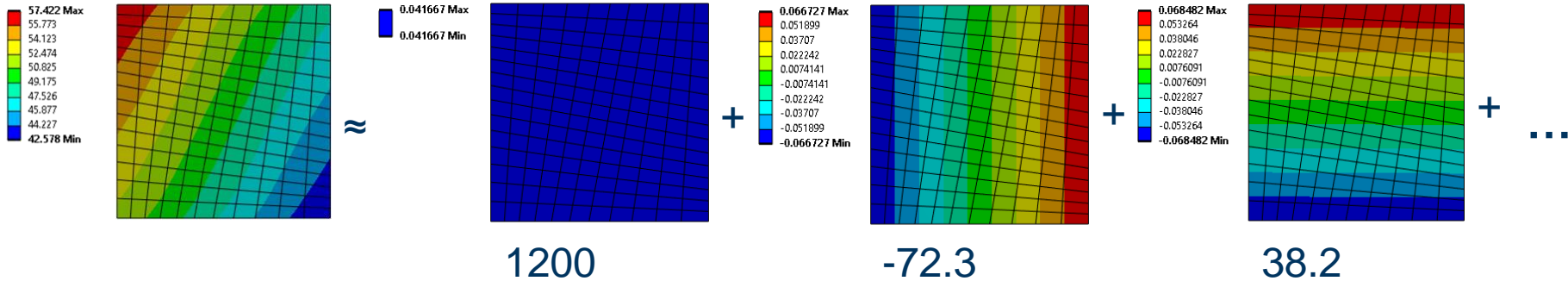
- $\|\mathbf{a}\| = \sqrt{\mathbf{a}^T \mathbf{a}}$
- E.g. $\mathbf{a} = \begin{Bmatrix} 2 \\ 1 \end{Bmatrix}$
- $\|\mathbf{a}\| = \sqrt{2 \cdot 2 + 1 \cdot 1} = \sqrt{5}$
- „L2-Norm“, Euclidian norm



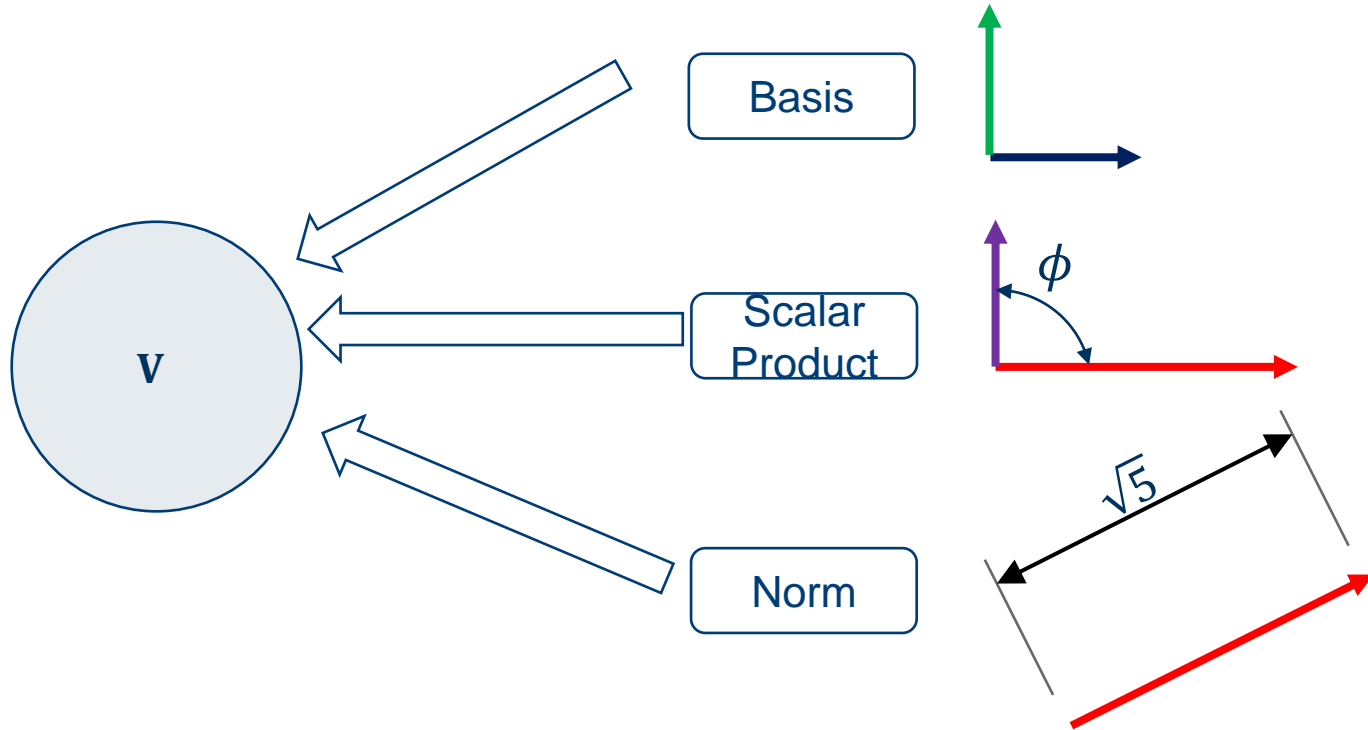
Vector Space V



Normalization of Basis Vectors – Normalized to 1

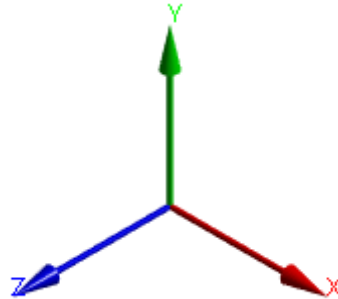


Vector Space V



Vector Space V

Engineers...

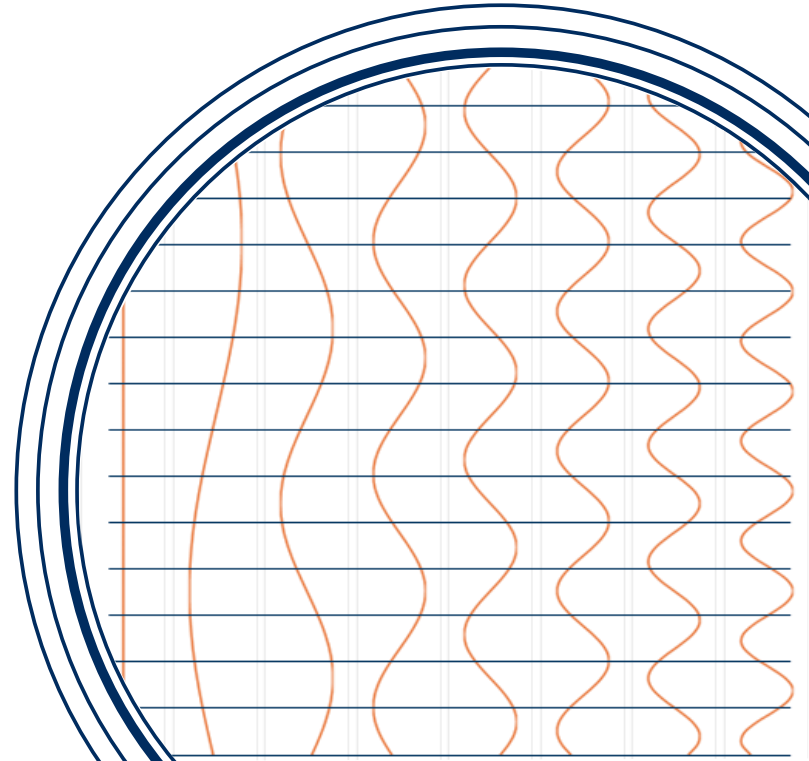


Discrete Fourier Transformation and Vector Space



CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



Discrete Fourier Transformation

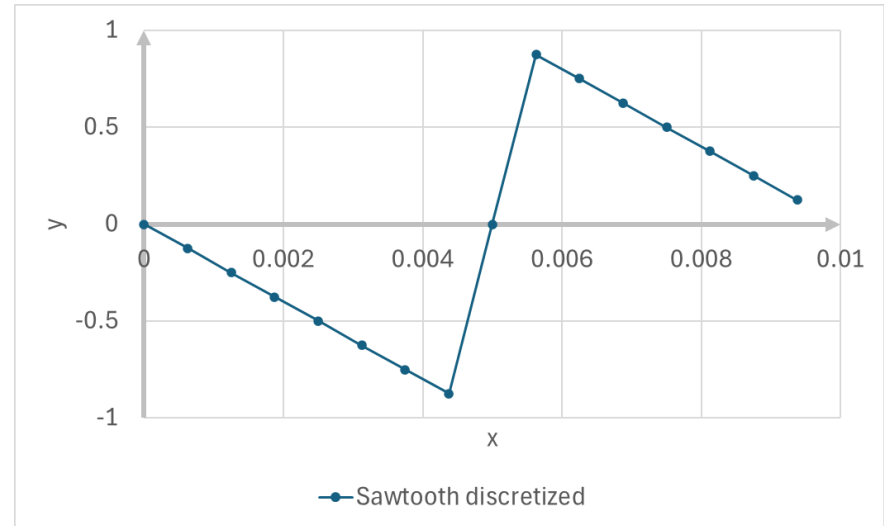
...is some kind of model order reduction



Discretized

- $\mathbf{y} = \{y_0, \dots, y_{N-1}\} \quad y \in \mathbb{R}^N$
- N Number of timepoints

→ From infinite to N 😊



Discrete Fourier Transformation

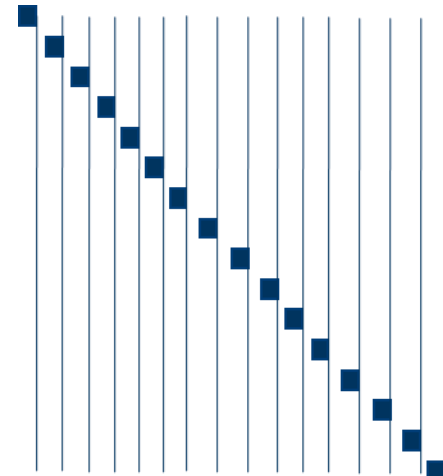


...is some kind of model order reduction

- Basis that we have intuitively assumed

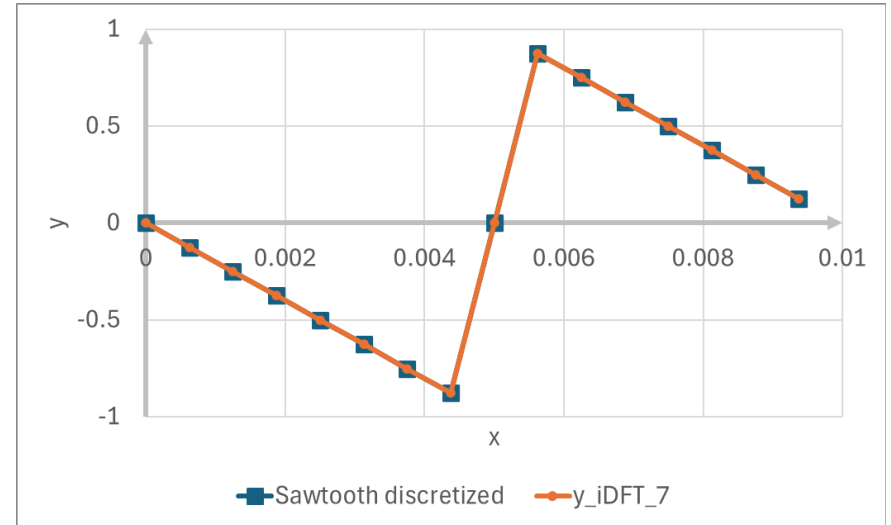
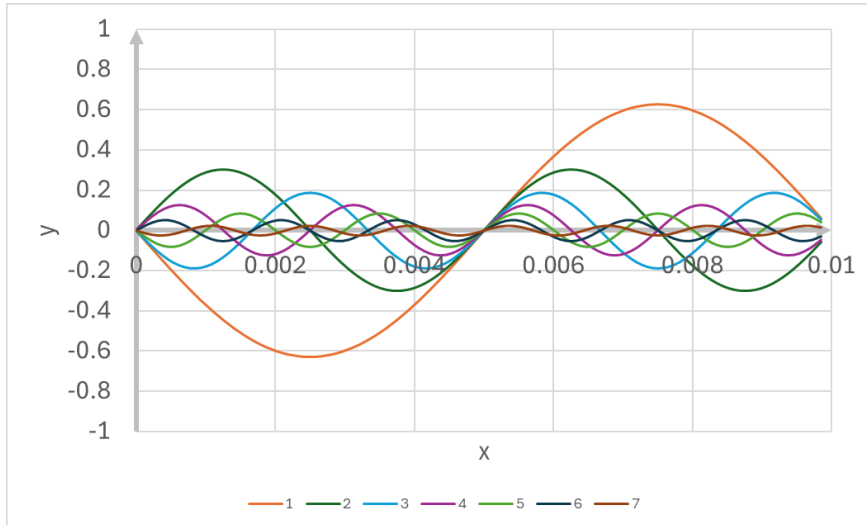
• **I**

1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1



Discrete Fourier Transformation

...is some kind of model order reduction



Discrete Fourier Transformation

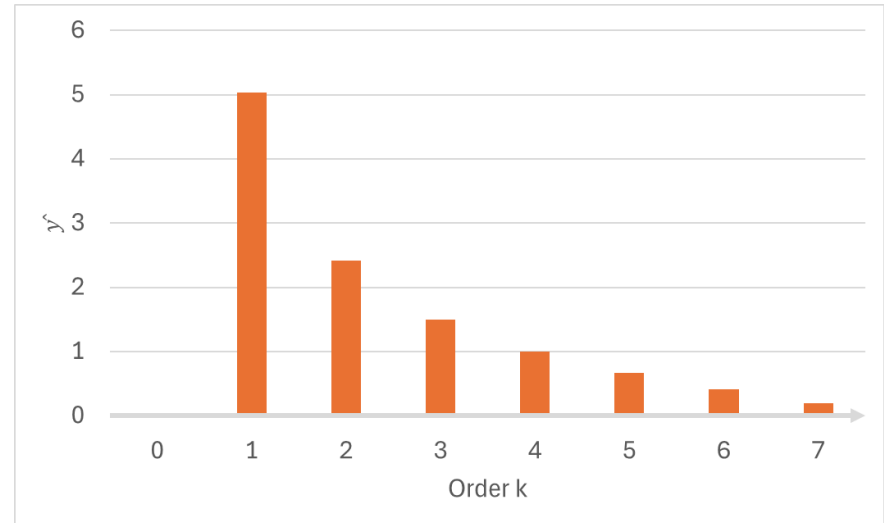
...is some kind of model order reduction



Discrete Fourier Transformation

- In matrix notation
 - $\hat{y} = \Phi^T y$

Projection!



Discrete Fourier Transformation

...is some kind of model order reduction



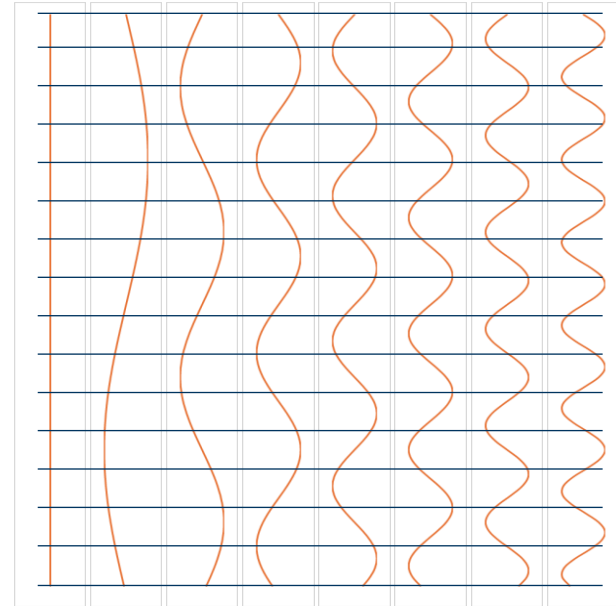
Discrete Fourier Transformation

- In matrix notation
 - $\hat{\mathbf{y}} = \mathbf{\Phi}^T \mathbf{y}$

Projection!

- **Change of basis**

Φ



Discrete Fourier Transformation

...is some kind of model order reduction



The basis is
orthonormal 😊

$$\Phi^T \Phi$$

1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0

Discrete Fourier Transformation

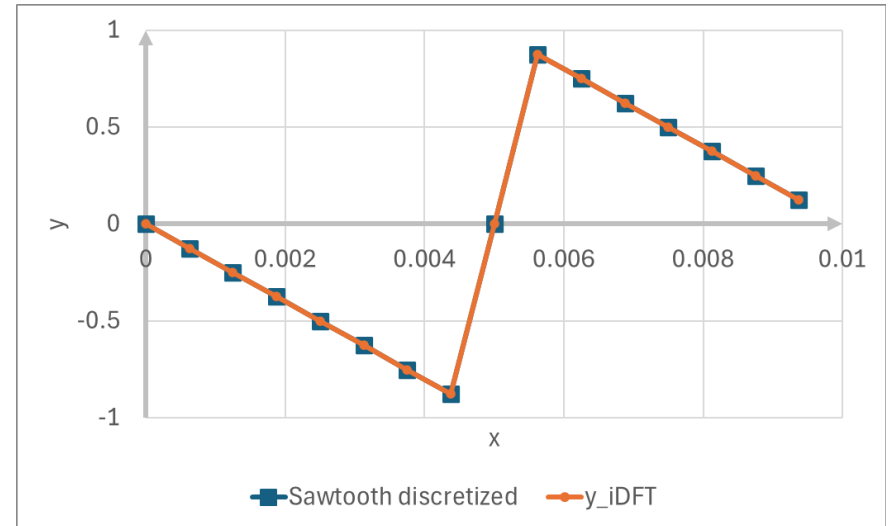
...is some kind of model order reduction



Inverse Discrete Fourier Transformation

- In matrix notation
 - $\mathbf{y} = [\Phi^T]^{-1} \hat{\mathbf{y}}$
 - $[\Phi^T]^{-1} = [\Phi^T]^T = \Phi$
 - $\mathbf{y} = \Phi \hat{\mathbf{y}}$

Expansion!



Discrete Fourier Transformation

...is some kind of model order reduction



Possibility to reduce the dimension

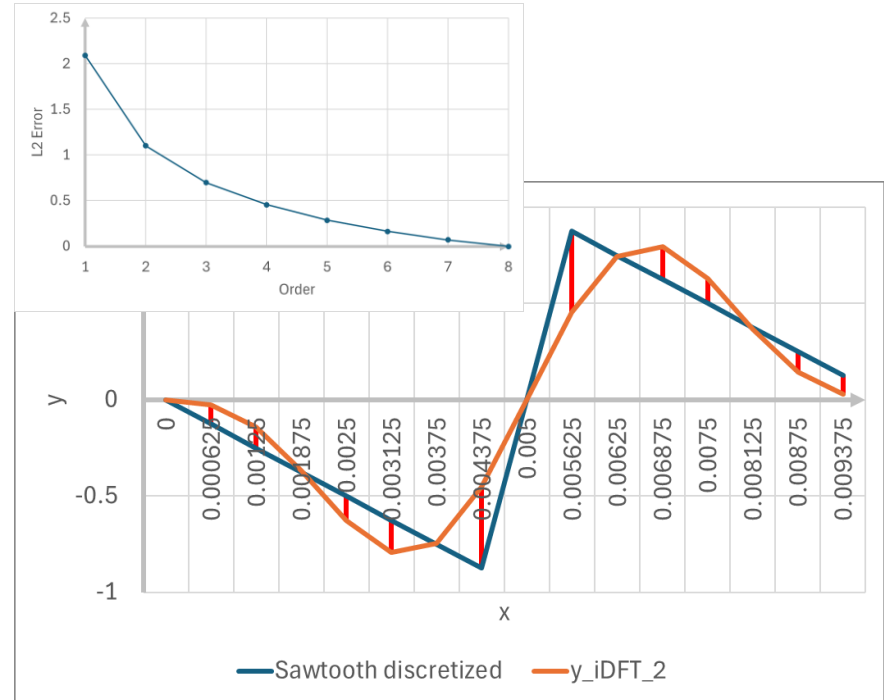
- by taking less Fourier coefficients

Projection

- to a truncated subspace

Error

- often measured by the L2-Norm of the difference



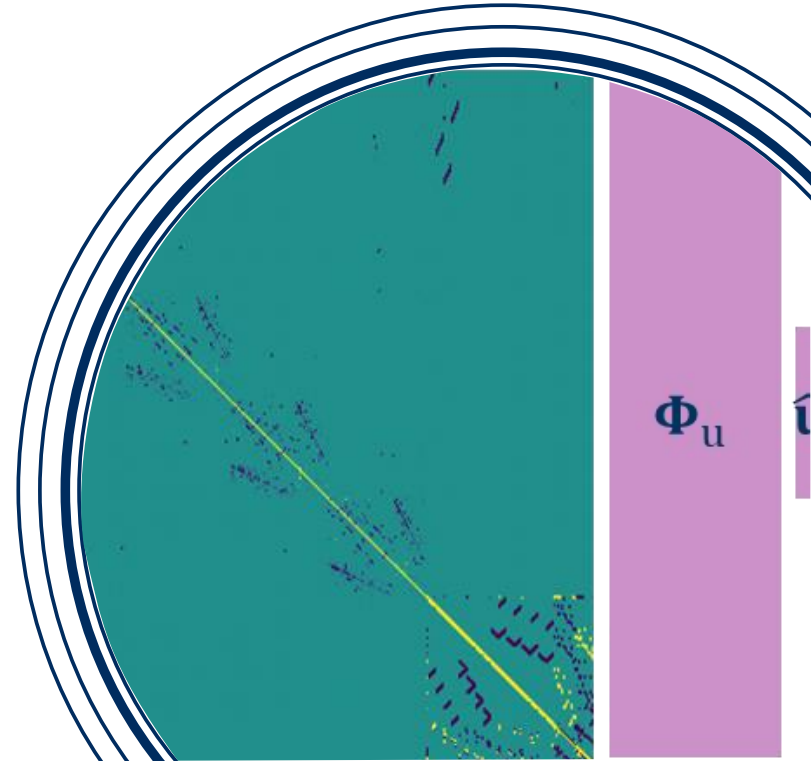
Link to Model Order Reduction

PCB Model



CADFEM®

Ansys / APEX CHANNEL PARTNER



PCB Model

Discretization

Structural model

Linear elements

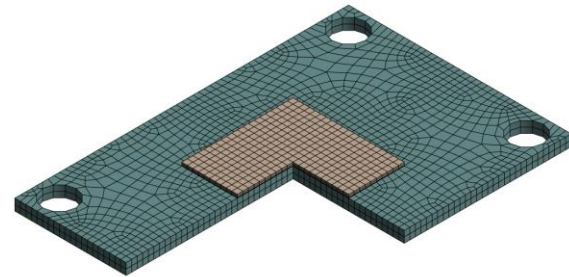
- 7383 nodes
- 5104 elements

3 Degrees of freedom per node

- u_x, u_y, u_z

Displacement vector

$$\bullet \mathbf{u} = \begin{Bmatrix} u_{x_1} \\ u_{y_1} \\ u_{z_1} \\ \vdots \\ u_{y_N} \\ u_{z_N} \end{Bmatrix}$$



PCB Model

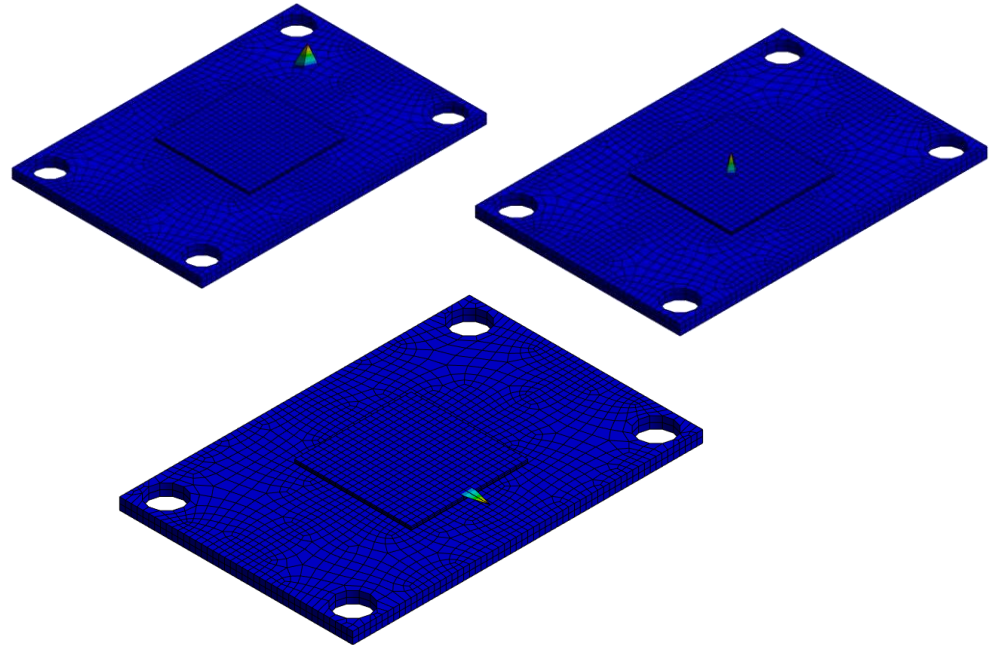


Vector Space

- Vector space of dimension
 - $N = 3 \cdot 7383 = 22149$
 - Euclidian basis
 - $\mathbf{I} \in \mathbb{R}^{N \times N}$



- Exemplary base vectors



PCB Model

Stiffness Matrix K

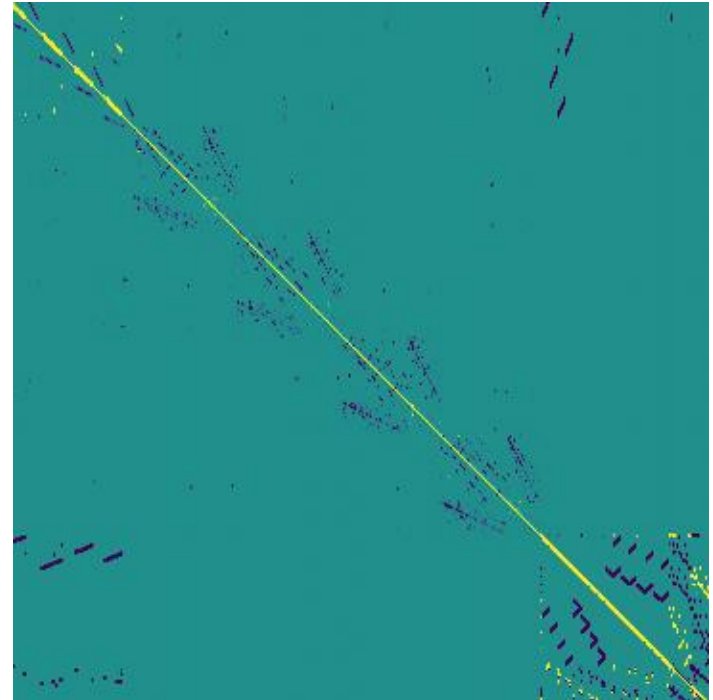
Symmetric

Positive definite

Sparse



N

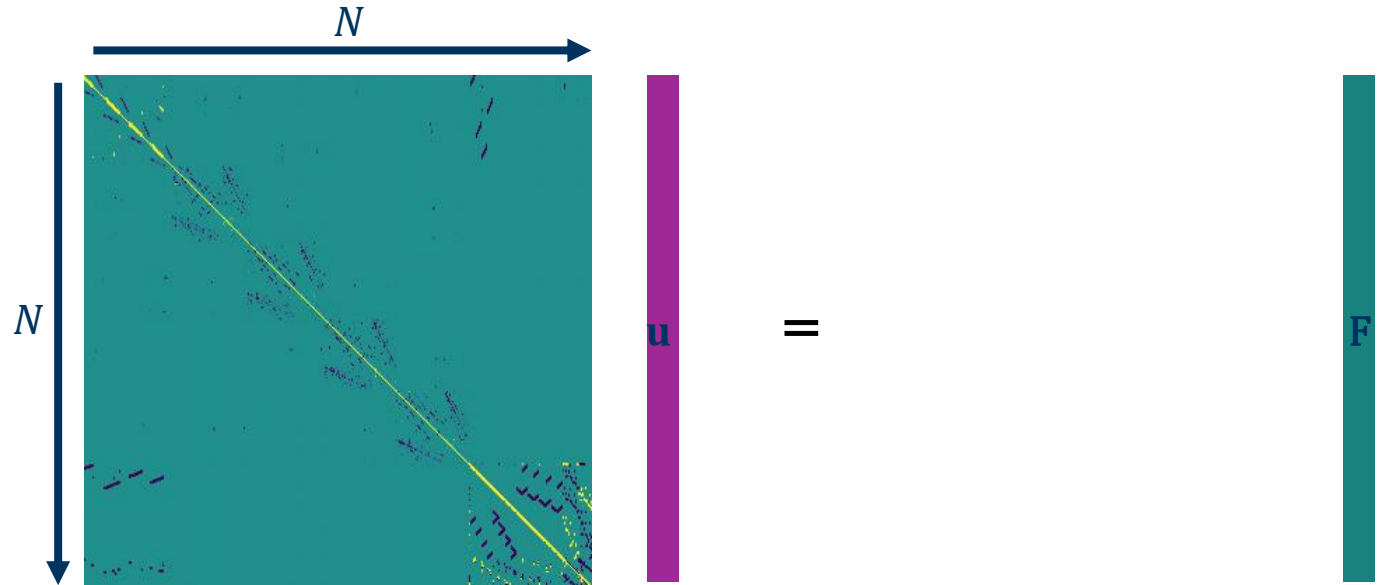


PCB Model

Describing Equations



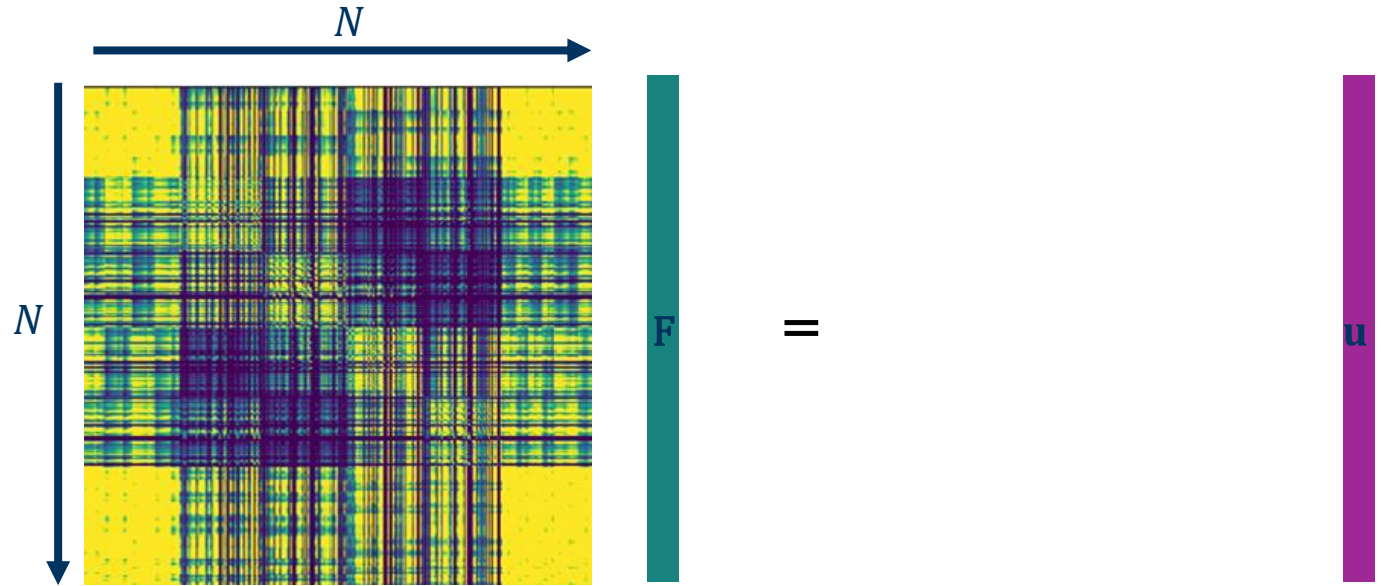
$\mathbf{Ku} = \mathbf{F}$, with external force vector \mathbf{F}



PCB Model

Solving

$$\mathbf{K}^{-1}\mathbf{F} = \mathbf{u}$$



PCB Model



Projection of Displacements

Project the displacements

- onto a smaller subspace of dimension $n \ll N$

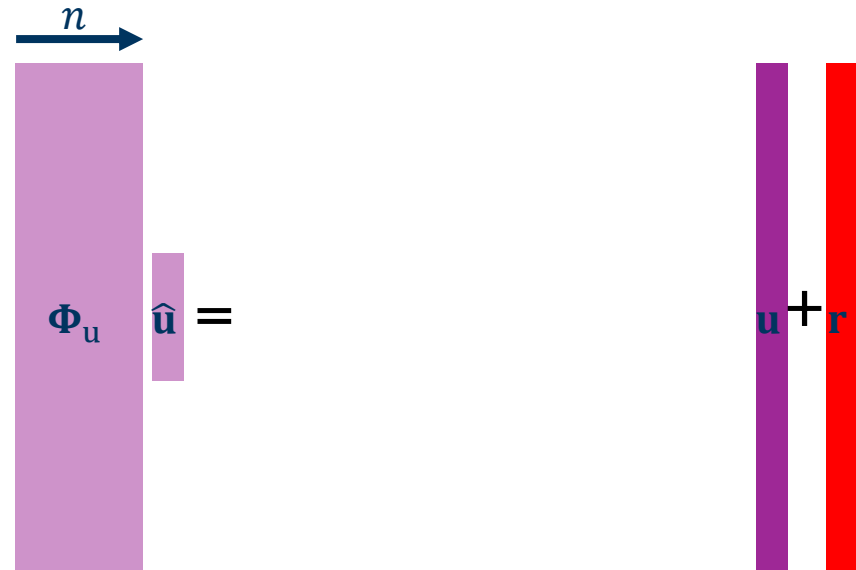
$$\mathbf{u} = \Phi_u \hat{\mathbf{u}} + \mathbf{r}$$

- As it is only an approximation, the residual \mathbf{r} is introduced

$$\mathbf{K}\mathbf{u} = \mathbf{F}$$

- $\mathbf{K}\Phi_u(\hat{\mathbf{u}} + \mathbf{r}) = \mathbf{F} - \mathbf{K}\Phi_u\mathbf{r}$
- $\mathbf{K}\Phi_u\hat{\mathbf{u}} = \mathbf{F} - \mathbf{K}\Phi_u\mathbf{r}$

$$\mathbf{K}\Phi_u\hat{\mathbf{u}} = \mathbf{F} - \tilde{\mathbf{r}}$$

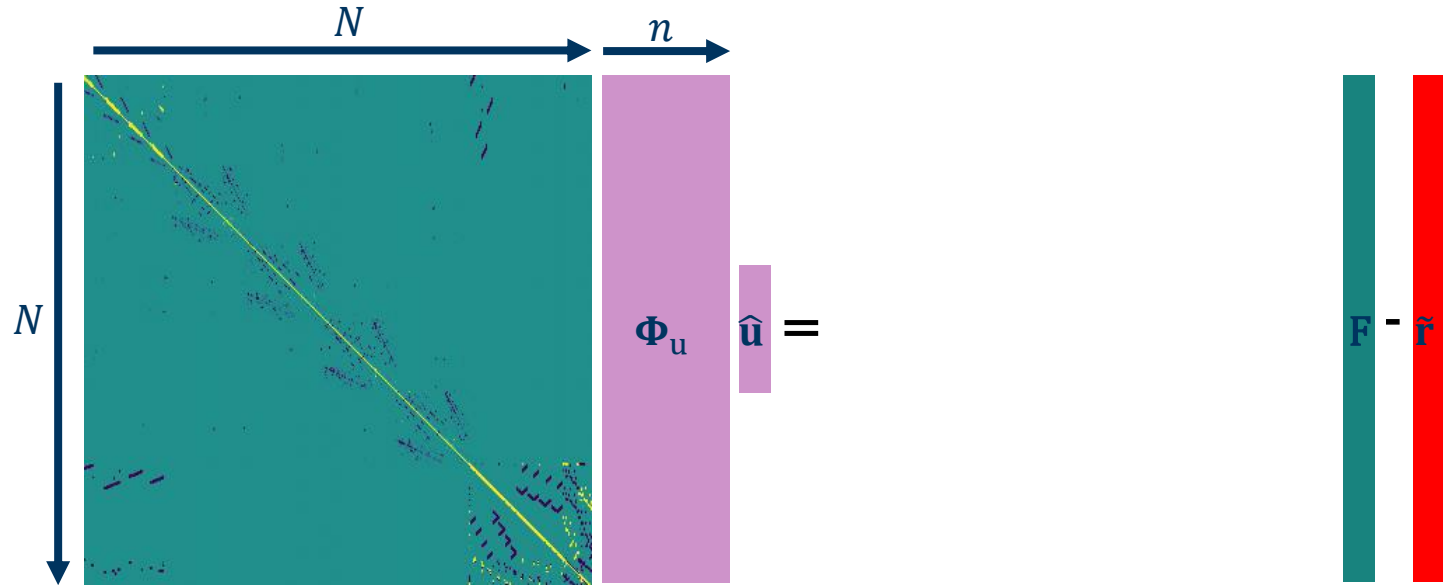


PCB Model

Projection of Displacements



$$\mathbf{K}\Phi_{\mathbf{u}}\hat{\mathbf{u}} = \mathbf{F} - \tilde{\mathbf{r}}$$



Galerkin Condition

$$\mathbf{K}\Phi_{\mathbf{u}}\hat{\mathbf{u}} = \mathbf{F} - \tilde{\mathbf{r}}$$

Galerkin condition

- The residual $\tilde{\mathbf{r}}$ is kept orthogonal to the subspace $\Phi_{\mathbf{u}}$

$$\Phi_{\mathbf{u}}^T \tilde{\mathbf{r}} = \mathbf{0}$$

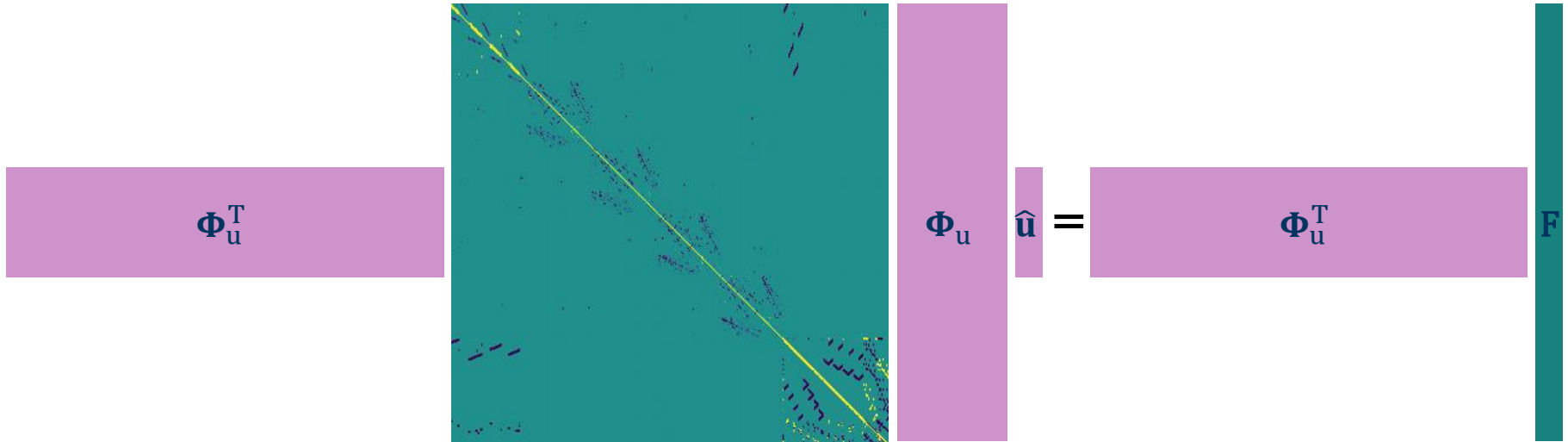
- Multiply by $\Phi_{\mathbf{u}}^T$
- $\Phi_{\mathbf{u}}^T \mathbf{K}\Phi_{\mathbf{u}}\hat{\mathbf{u}} = \Phi_{\mathbf{u}}^T \mathbf{F} - \Phi_{\mathbf{u}}^T \tilde{\mathbf{r}}$
- $\underbrace{\Phi_{\mathbf{u}}^T \mathbf{K}\Phi_{\mathbf{u}}}_{\hat{\mathbf{K}}}\hat{\mathbf{u}} = \underbrace{\Phi_{\mathbf{u}}^T \mathbf{F}}_{\hat{\mathbf{F}}}$

PCB Model

Reduced Order Model



- $\Phi_u^T K \Phi_u \hat{u} = \Phi_u^T F$

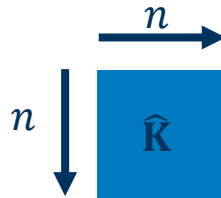


PCB Model

Reduced Order Model



$$\bullet \underbrace{\Phi_u^T K \Phi_u}_{\hat{K}} \hat{u} = \underbrace{\Phi_u^T F}_{\hat{F}}$$

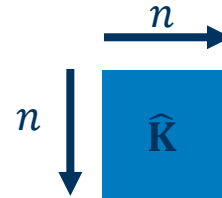


=



Generalized...

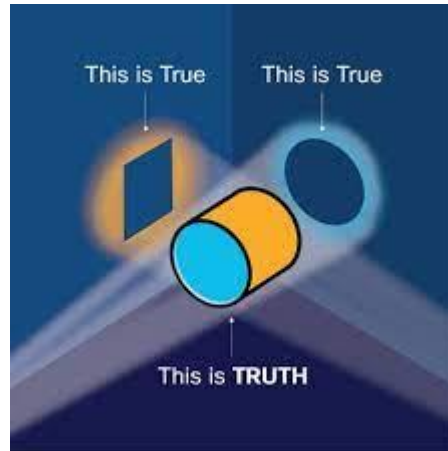
- stiffness matrix $\hat{\mathbf{K}}$
- force vector $\hat{\mathbf{F}}$
- displacement vector $\hat{\mathbf{u}}$



PCB Model



Idea of Projection Based Model Order Reduction



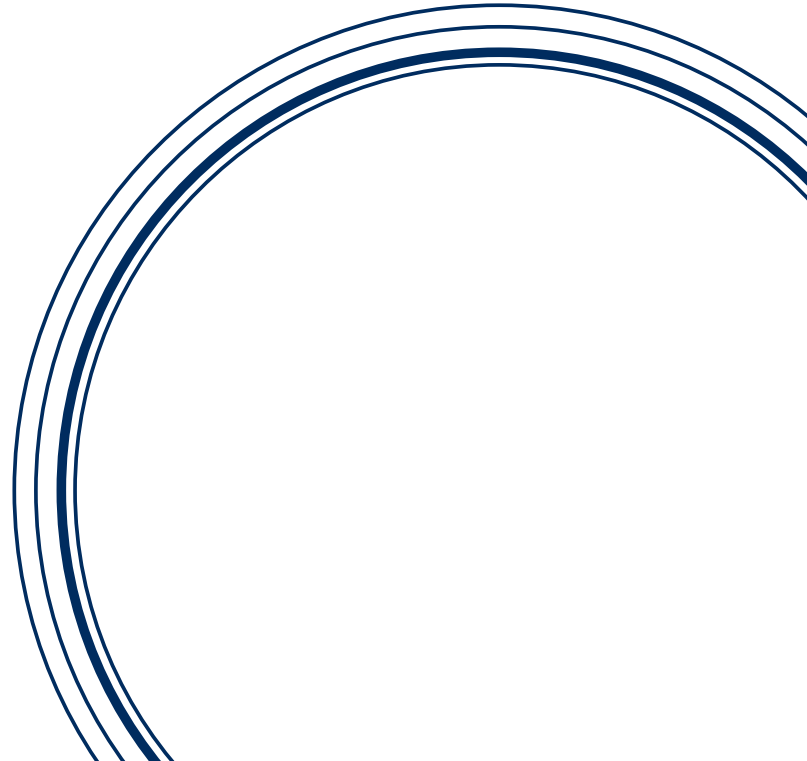
<https://www.facebook.com/examath/photos/a.166108407455452/1180064439393172/?type=3>

How to find a good Subspace



CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



Based on System Matrices

- Modal Subspace
- Krylov Subspace

Based on Simulation Results

- Gram Schmidt Orthogonalization
- Proper Orthogonal Decomposition/ Principal Component Analysis/ Method of Snapshots

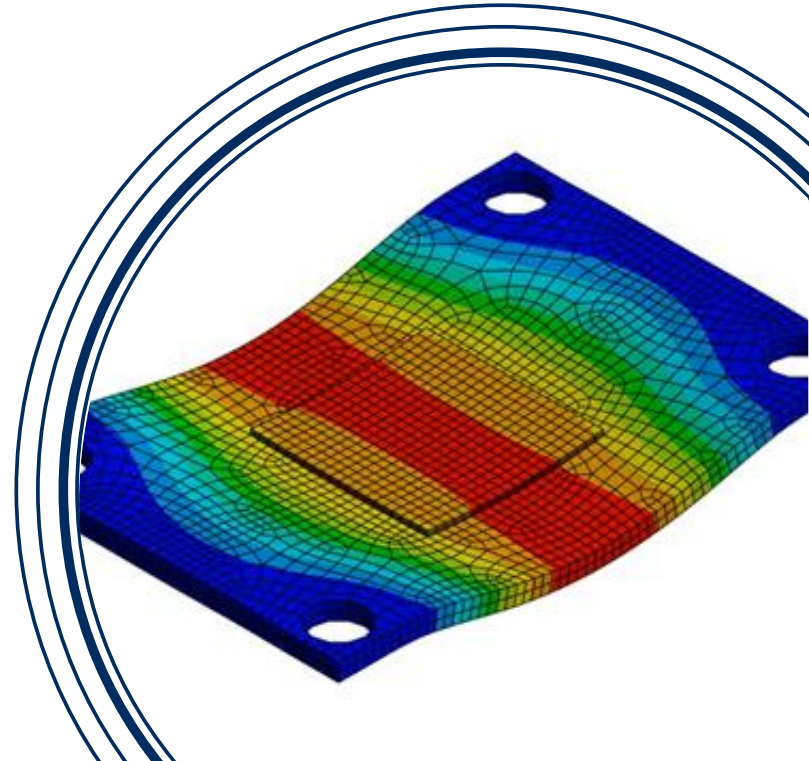
How to find a good Subspace

Modal Analysis



CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



“What the system wants to do” – Free Vibrations

Equation of motion

- $\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{F}_{\text{ext}}$
- Damping is neglected
- Independent of external force

$$\rightarrow \mathbf{M}\ddot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{0}$$

- Displacement vector $\mathbf{u} \in \mathbb{R}^N$
- Velocity vector $\dot{\mathbf{u}} \in \mathbb{R}^N$
- Acceleration vector $\ddot{\mathbf{u}} \in \mathbb{R}^N$
- External Force $\mathbf{F}_{\text{ext}} \in \mathbb{R}^N$

- Mass Matrix $\mathbf{M} \in \mathbb{R}^{N \times N}$
- Stiffness Matrix $\mathbf{K} \in \mathbb{R}^{N \times N}$
- Damping Matrix $\mathbf{C} \in \mathbb{R}^{N \times N}$

Modal Analysis



“What the system wants to do” – Free Vibrations

Equation of motion

- $\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{F}_{\text{ext}}$
- Damping is neglected
- Independent of external force

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{0}$$

For a linear system, free vibrations are harmonic

- $\mathbf{u} = \Phi_i \cos \omega_i t$
- Decomposition of i -1-DOF-Oscillators

- i -th modeshape Φ_i
- i -th natural frequency ω_i
- Time t

“What the system wants to do” – Free Vibrations

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{0}$$

- with $\ddot{\mathbf{u}} = -\omega^2\mathbf{u}$

$$(-\omega^2\mathbf{M} + \mathbf{K})\boldsymbol{\phi}_i = \mathbf{0}$$

- This equation is satisfied if
 - $\boldsymbol{\phi}_i = \mathbf{0}$
 - trivial, not of interest
 - Determinant of $(-\omega^2\mathbf{M} + \mathbf{K})$ is $\mathbf{0}$

(generalized) eigenvalue problem

- Outputs
 - n mode shapes $\boldsymbol{\Phi} = [\boldsymbol{\Phi}_1 \quad \dots \quad \boldsymbol{\Phi}_n]$
 - n natural frequencies $\boldsymbol{\omega} = \{\omega_1 \quad \dots \quad \omega_n\}$

Modal Analysis



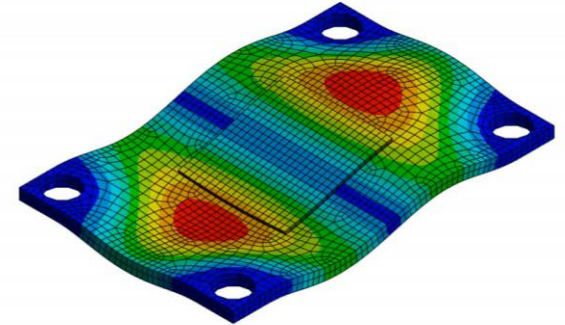
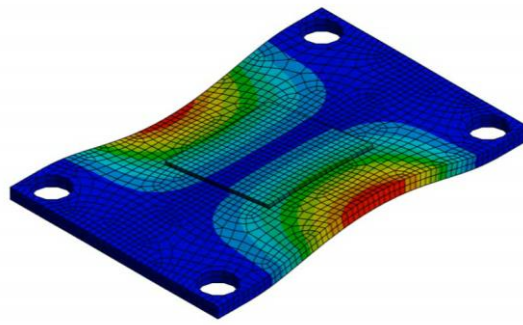
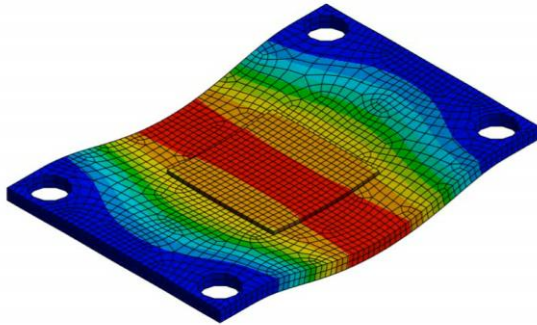
CADFEM®

“What the system wants to do” – Free Vibrations

Mode 1, $f_1 = 3.1\text{kHz}$

Mode 2, $f_2 = 4.3\text{kHz}$

Mode 3, $f_3 = 7.3\text{kHz}$



Modal Analysis



“What the system wants to do” – Free Vibrations

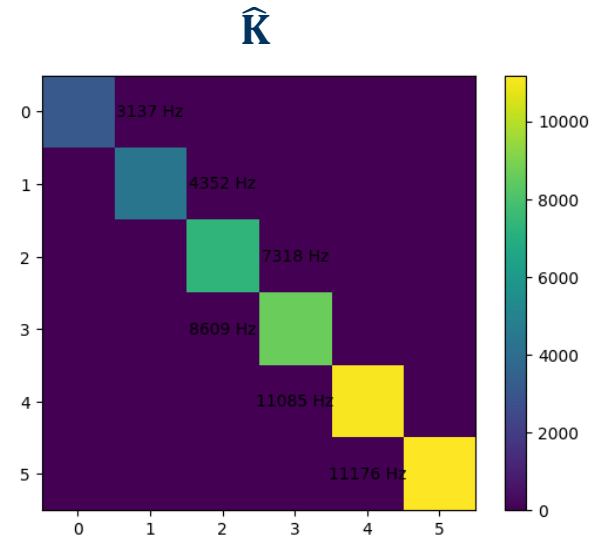
Implemented in all commercial FE-Codes

Number of mode shapes?

- The natural frequencies are ordered, from low to high frequencies
- In general: Dimension of the vector space of the model
 - → The same vector space is spanned
- Rule of thumb:
 - Consider mode shapes up to twice the excitation frequency
 - → Modal Truncation

Properties of mode shapes

- Orthogonal basis
- System matrices (**K** and **M**) are decoupled
 - Modal Superposition
 - With “Mass normalization”
 - $\Phi^T \mathbf{M} \Phi = \text{diag}(1)$, scalar product
 - $\Phi^T \mathbf{K} \Phi = \text{diag}(\omega^2)$

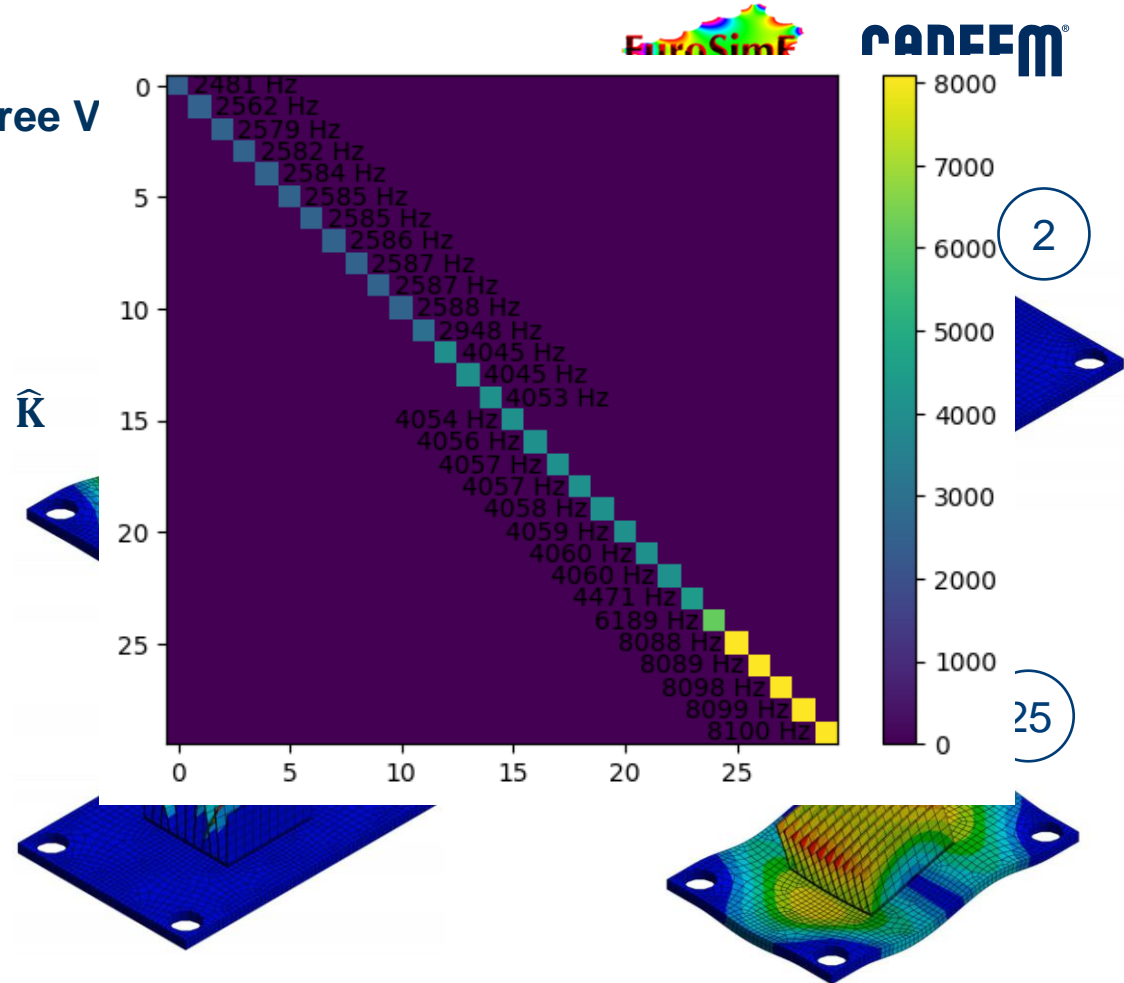


Modal Analysis

“What the system wants to do” – Free V

Drawbacks

- Small structures → many modes
- Excitation is not considered
 - Many inner modes
- Only for linear dynamics
 - Commonly used for structural



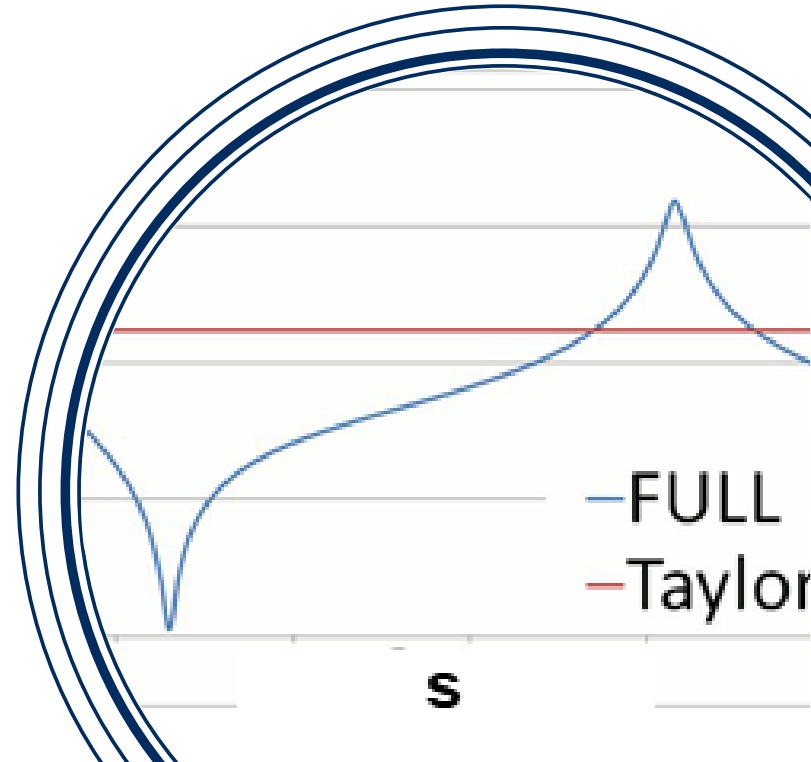
How to find a good Subspace

Krylov Subspace - Implicit Moment Matching



CADFEM®

Ansys / APEX
CHANNEL PARTNER



General definition of Krylov Subspace

- $\mathcal{K} = \mathcal{K}(\mathbf{A}, \mathbf{q}) = \text{span}\{\mathbf{q}, \mathbf{A}\mathbf{q}, \dots, \mathbf{A}^{m-1}\mathbf{q}\}$

Used in many algorithms

- Arnoldi (solution of eigenvalue problems)
- Lanczos (solution of eigenvalue problems)
- GMRES (approximate solution of systems of linear equations)
- QMR (approximate solution of systems of linear equations)
- ...

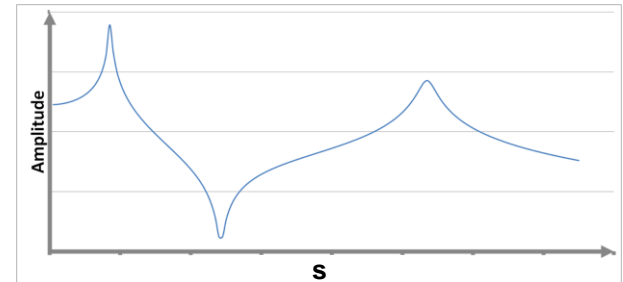
Moment Matching



What is a Moment in this Context?

General transfer function

- in Laplace domain
- Fourier integral is a special case with $s = i\omega$
- $(s^2\mathbf{M} - \mathbf{K})\mathbf{u} = \mathbf{F}_{\text{ext}}$
- $\underbrace{(s^2\mathbf{M} - \mathbf{K})^{-1}}_{\mathbf{K}_{\text{eq}}(s)} \mathbf{F}_{\text{ext}} = \mathbf{u}$



Moment Matching

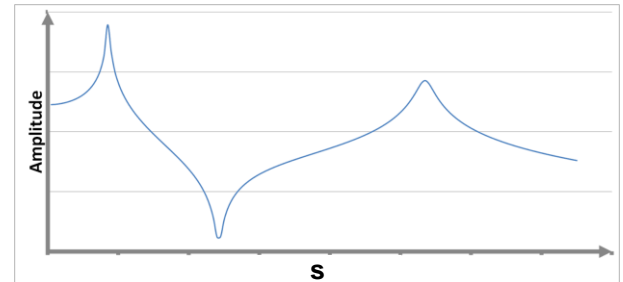


What is a Moment in this Context?

$$\underbrace{(s^2 \mathbf{M} - \mathbf{K})^{-1}}_{\mathbf{K}_{eq}(s)} \mathbf{F}_{ext} = \mathbf{u}$$

Taylor series

- around s_0^2
- $\mathbf{u} = \sum_i \mathbf{m}_i (s^2 - s_0^2)^i$
 - Hint: the i -th derivative in the Laplace domain is just $s^i \cdot f(s)$
 - \mathbf{m}_i are called moments of the transfer function



Moment Matching

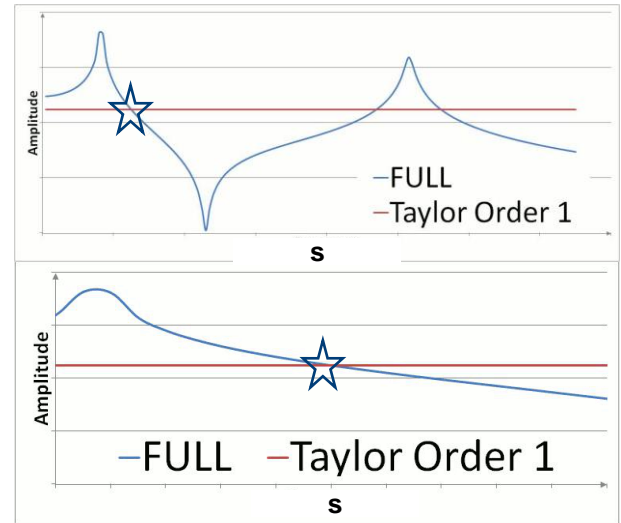
Explicit Moment Matching



$$\mathbf{u} = \sum_i \mathbf{m}_i (s^2 - s_0^2)^i$$

Explicit calculation of moments is numerically unstable

- $\mathbf{m}_i = \tilde{\mathbf{M}}^i \tilde{\mathbf{F}}$
- $\tilde{\mathbf{M}}^i = \left[-\mathbf{K}_{\text{eq}(s_0)}^{-1} \mathbf{M} \right]^i$
- $\tilde{\mathbf{F}} = \mathbf{K}_{\text{eq}(s_0)}^{-1} \mathbf{F}_{\text{ext}}$



Moment Matching

Implicit Moment Matching



Explicit Moments

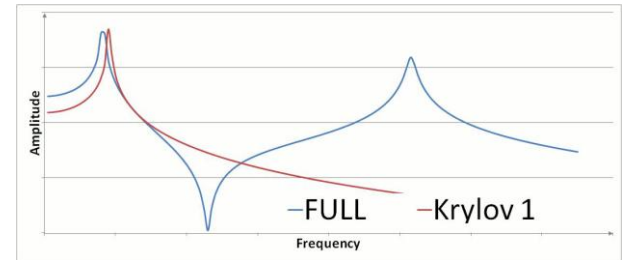
- $\mathbf{m}_i = \tilde{\mathbf{M}}^i \tilde{\mathbf{F}}$
- $\tilde{\mathbf{M}}^i = \left[-\mathbf{K}_{\text{eq}(s_0)}^{-1} \mathbf{M} \right]^i$
- $\tilde{\mathbf{F}} = \mathbf{K}_{\text{eq}(s_0)}^{-1} \mathbf{F}_{\text{ext}}$

Krylov subspace definition

- $\mathcal{K} = \mathcal{K}(\mathbf{A}, \mathbf{q}) = \text{span}\{\mathbf{q}, \mathbf{A}\mathbf{q}, \dots, \mathbf{A}^{m-1}\mathbf{q}\}$
- $\mathbf{A} = \tilde{\mathbf{M}}$
- $\mathbf{q} = \tilde{\mathbf{F}}$

The moments lie in the Krylov Subspace!

- The first moment \mathbf{q} is just the solution at the expansion point

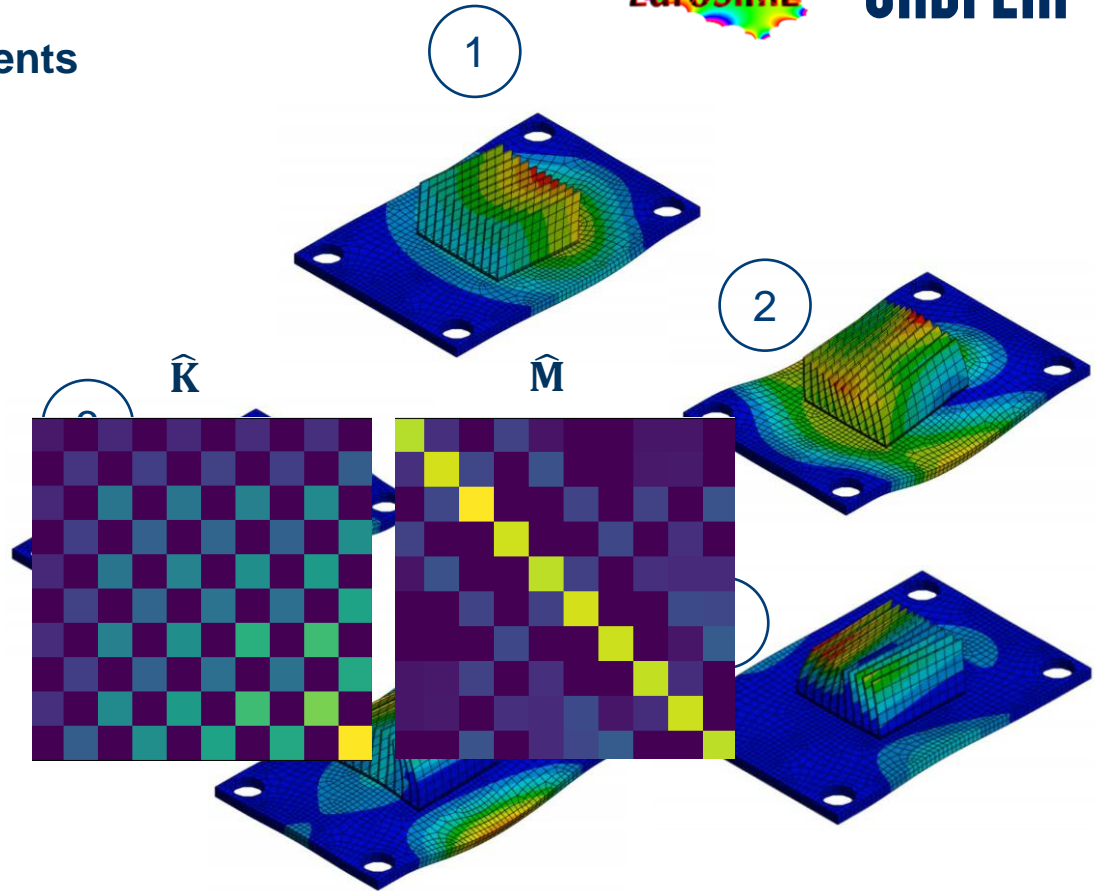


Moment Matching

Implicit Moment Matching - Comments



- The load is included!
- No decoupling of the reduced matrices



Moment Matching



Implicit Moment Matching - Comments

Implicit moment matching is not limited to structural dynamics

Expansion point should be set according to the frequency range of interest

It is possible to use multiple expansion points

There is no established rule how many vectors should be considered

Can be expanded to “parametric model order reduction” – the Taylor expansion is then done also for the parameter

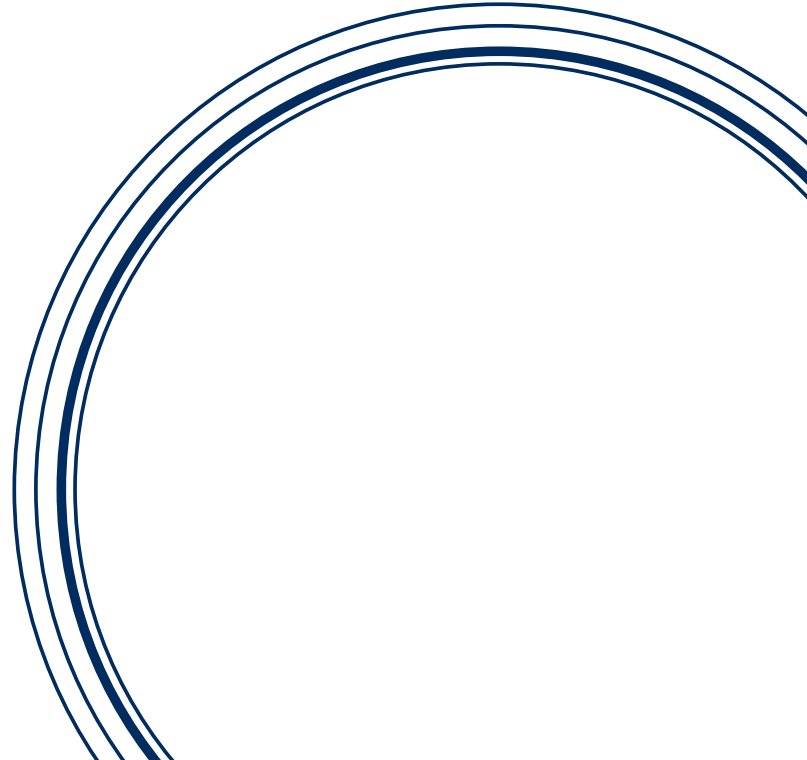
How to find a good Subspace

Based on Simulation Results



CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



Methods to Determine Subspaces

Based on Simulation Results



Snapshot matrix

- Do a calculation for m timesteps and assemble the results of interest $\mathbf{y} \in \mathbb{R}^N$ in a $\mathbf{S} = [\mathbf{y}_1, \dots, \mathbf{y}_n] \in \mathbb{R}^{N \times m}$

The snapshots define the vector space of the solution – how to find an orthonormal basis?

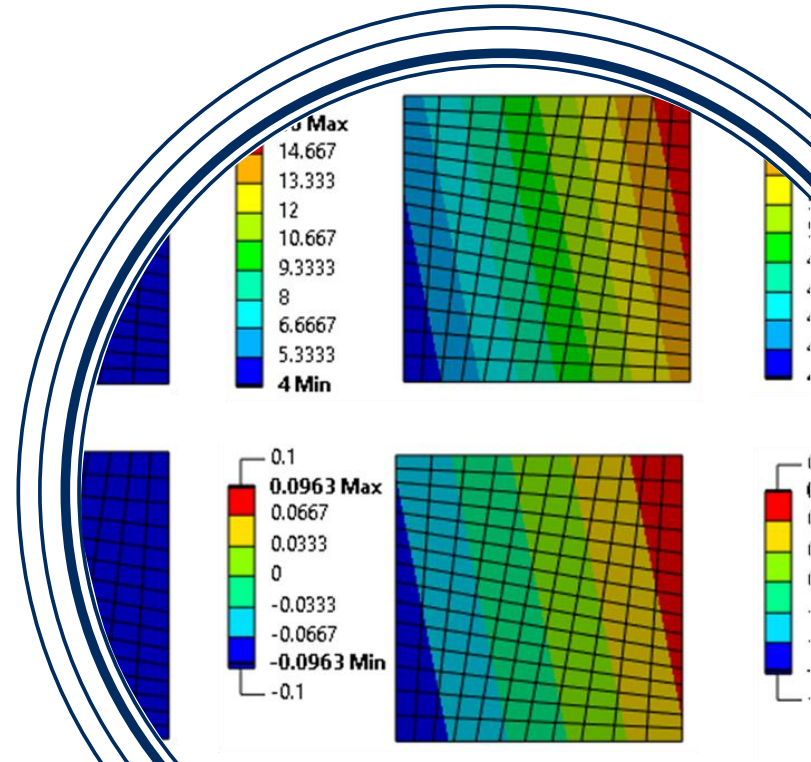
How to find a good Subspace

Gram Schmidt Orthogonalization



CADFEM®

ANSYS / APEX CHANNEL PARTNER



Gram Schmidt Orthogonalization



Given

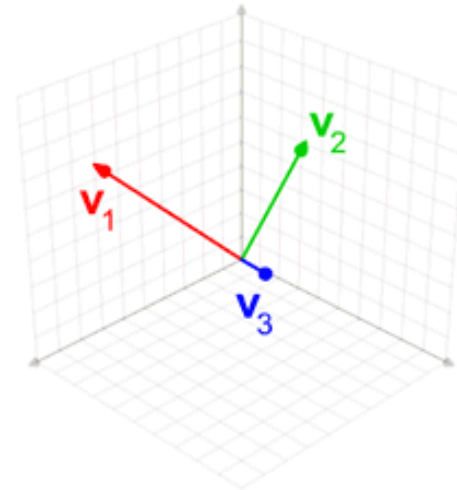
- m vectors \mathbf{v}_i in \mathbb{R}^N

Target

- m orthonormal vectors \mathbf{u}_i in \mathbb{R}^N

Algorithm

- $\mathbf{u}_1 = \frac{\mathbf{v}_1}{\|\mathbf{v}_1\|}$ Normalization of vector \mathbf{v}_1
- $\mathbf{u}'_2 = \mathbf{v}_2 - \frac{\langle \mathbf{v}_2, \mathbf{u}_1 \rangle}{\langle \mathbf{u}_1, \mathbf{u}_1 \rangle} \mathbf{u}_1$ Orthogonalization of \mathbf{v}_2
- $\mathbf{u}_2 = \frac{\mathbf{u}'_2}{\|\mathbf{u}'_2\|}$ Normalization of vector \mathbf{u}'_2
- $\mathbf{u}'_3 = \mathbf{v}_3 - \frac{\langle \mathbf{v}_3, \mathbf{u}_1 \rangle}{\langle \mathbf{u}_1, \mathbf{u}_1 \rangle} \mathbf{u}_1 - \frac{\langle \mathbf{v}_3, \mathbf{u}_2 \rangle}{\langle \mathbf{u}_2, \mathbf{u}_2 \rangle} \mathbf{u}_2$ Orthogonalization of \mathbf{v}_3
- $\mathbf{u}_3 = \frac{\mathbf{u}'_3}{\|\mathbf{u}'_3\|}$ Normalization of vector \mathbf{u}'_3
- ...
- $\mathbf{u}'_m = \mathbf{v}_m - \sum_{i=1}^{m-1} \frac{\langle \mathbf{v}_m, \mathbf{u}_i \rangle}{\langle \mathbf{u}_i, \mathbf{u}_i \rangle} \mathbf{u}_i$ Orthogonalization of \mathbf{v}_m
- $\mathbf{u}_m = \frac{\mathbf{u}'_m}{\|\mathbf{u}'_m\|}$ Normalization of vector \mathbf{u}'_m



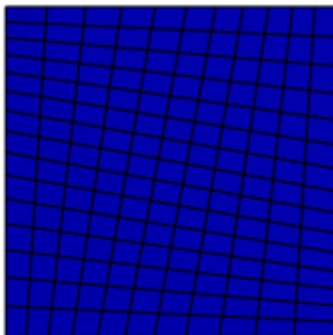
https://upload.wikimedia.org/wikipedia/commons/e/ee/Gram-Schmidt_orthonormalization_process.gif

Gram Schmidt Orthogonalization

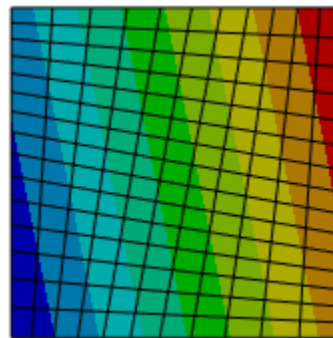


Snapshots

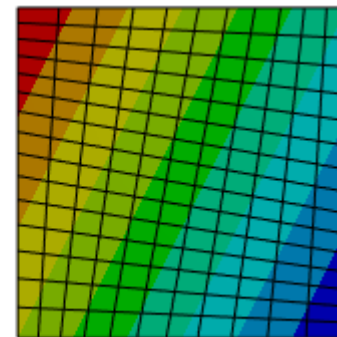
1 Max
1 Min



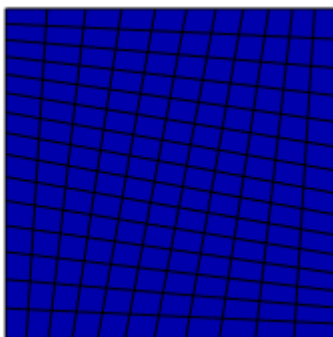
16 Max
14.667
13.333
12
10.667
9.3333
8
6.6667
5.3333
4 Min



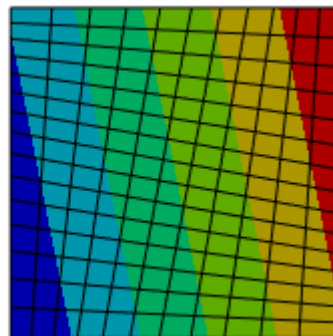
57.5 Max
55.833
54.167
52.5
50.833
49.167
47.5
45.833
44.167
42.5 Min



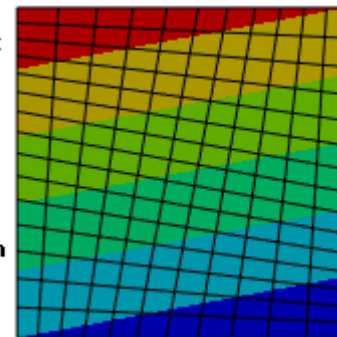
0.051 Max
0.051 Min



0.1
0.0963 Max
0.0667
0.0333
0
-0.0333
-0.0667
-0.0963 Min
-0.1



0.1
0.0972 Max
0.0667
0.0333
0
-0.0333
-0.0667
-0.0972 Min
-0.1



Applications

Find an orthonormal basis for given vectors

How to truncate the basis?

- Engineering Knowledge: Select appropriate snapshots to calculate the basis

Used in different numerical algorithms (e.g. for the calculation of Krylov subspaces)

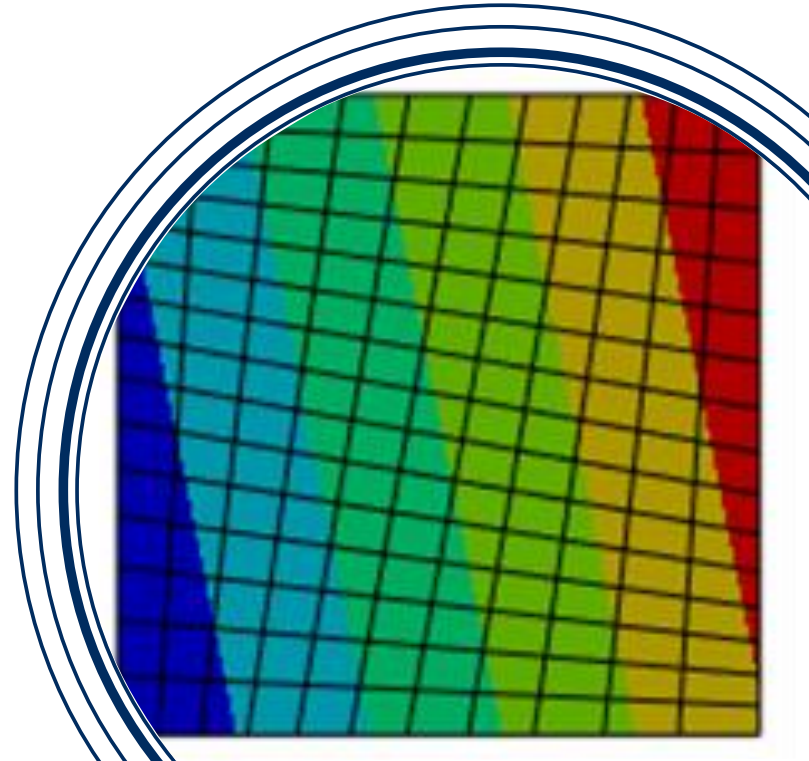
How to find a good Subspace

Proper Orthogonal Decomposition



CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



Target

Find the best linear subspace for the approximation of the data

$$\mathbf{S} = [\mathbf{y}_1, \dots, \mathbf{y}_n] \in \mathbb{R}^{N \times m}$$

Principal Component Analysis

Compute the eigenvalue decomposition of $\mathbf{Y} = \mathbf{S}\mathbf{S}^T \in \mathbb{R}^{N \times N}$

→ Sorted Eigenvalues $\lambda = \{\lambda_1, \dots, \lambda_N\}$ and Eigenvectors $\Psi = [\Psi_1, \dots, \Psi_N]$

→ Basisvectors $\Phi_i = \Psi_i \in \mathbb{R}^N$

Method of Snapshots

Compute the eigenvalue decomposition of $\mathbf{Y} = \mathbf{S}^T\mathbf{S} \in \mathbb{R}^{m \times m}$

→ Sorted Eigenvalues $\lambda = \{\lambda_1, \dots, \lambda_N\}$ and Eigenvectors $\Psi = [\Psi_1, \dots, \Psi_N]$

→ Basisvectors $\Phi_i = \mathbf{S}\Psi_i \in \mathbb{R}^N$

Best Linear Approximation

Take n basisvectors corresponding to the largest eigenvalues

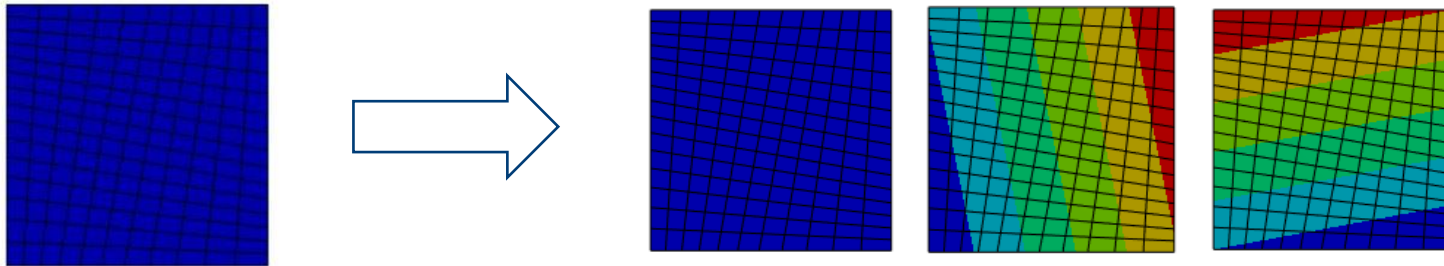
Use Cases

Principal Component Analysis

- Compute the eigenvalue decomposition of $\mathbf{Y} = \mathbf{S}\mathbf{S}^T \in \mathbb{R}^{N \times N}$
- Efficient if length N of snapshot vectors (e.g. locations) is low compared to count m of snapshots (e.g. timesteps)
→ Measurement data

Method of Snapshots

- Compute the eigenvalue decomposition of $\mathbf{Y} = \mathbf{S}^T\mathbf{S} \in \mathbb{R}^{m \times m}$
- Efficient if count m of snapshots (e.g. timesteps) is low compared to length N of snapshot vectors (e.g. locations)
→ Simulation data

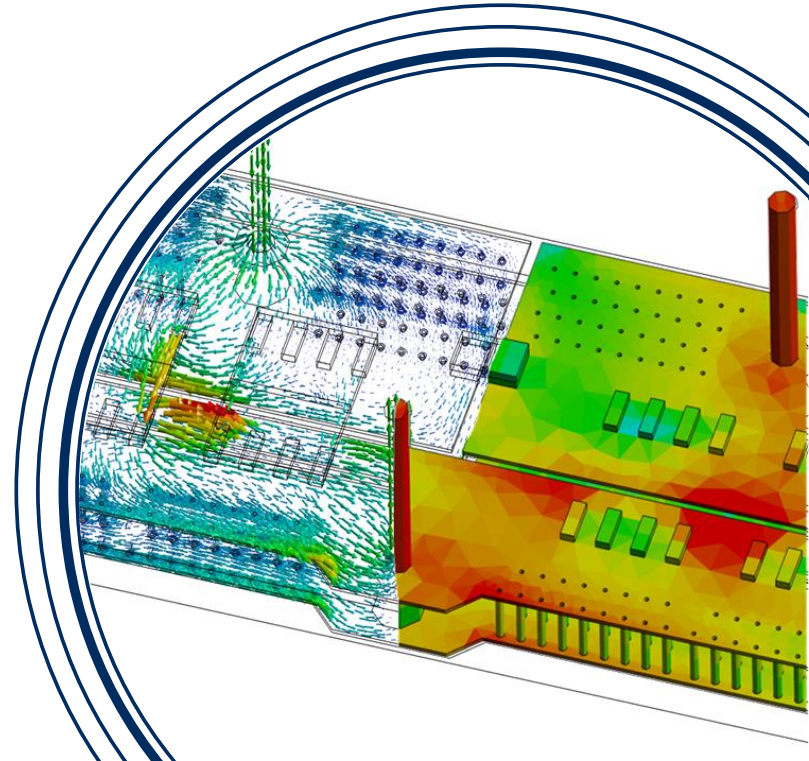


Summary

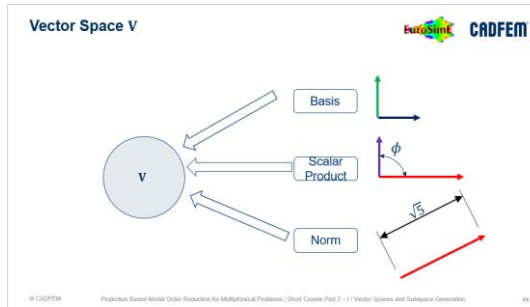


CADFEM[®]

Ansys / APEX
CHANNEL PARTNER



Summary



PCB Model Reduced Order Model

• $\Phi_u^T K \Phi_u \tilde{u} = \Phi_u^T F$

© CADFEM Projection Based Model Order Reduction for Multiphysical Problems | Short Course Part 2 – I | Vector Spaces and Subspace Generation 48

Modal Analysis

“What the system wants to do” – Free Vibrations

Mode 1, $f_1 = 3.1\text{kHz}$ Mode 2, $f_2 = 4.3\text{kHz}$ Mode 3, $f_3 = 7.3\text{kHz}$

© CADFEM Projection Based Model Order Reduction for Multiphysical Problems | Short Course Part 2 – I | Vector Spaces and Subspace Generation 74

Gram Schmidt Orthogonalization

© CADFEM Projection Based Model Order Reduction for Multiphysical Problems | Short Course Part 2 – I | Vector Spaces and Subspace Generation 88

PCB Model Reduced Order Model

• $\frac{\Phi_u^T K \Phi_u}{\tilde{k}} \tilde{u} = \frac{\Phi_u^T F}{\tilde{f}}$

© CADFEM Projection Based Model Order Reduction for Multiphysical Problems | Short Course Part 2 – I | Vector Spaces and Subspace Generation

Moment Matching

Nonlinear within ROM?

Session 18 Solder joint reliability simulation 1

10:45

Wednesday April 10 2024

11:05 20mn

Reduced-Order Model for Solder Balls – Potential of projection-based approaches for representing viscoplastic behavior

Mike Feuchter¹, Hanna Baumgartl¹, Martin Hanke¹, Sven Rzepka²

¹ CADFEM Germany GmbH
² Fraunhofer ENAS, Germany

Proper Orthogonal Decomposition Use Cases

Principal Component Analysis

- Compute the eigenvalue decomposition of $Y = SS^T \in \mathbb{R}^{m \times m}$
- Efficient if length N of snapshot vectors (e.g. locations) is low compared to count m of snapshots (e.g. timesteps)
- Measurement data

Method of Snapshots

- Compute the eigenvalue decomposition of $Y = S^T S \in \mathbb{R}^{m \times m}$
- Efficient if count m of snapshots (e.g. timesteps) is low compared to length N of snapshot vectors (e.g. locations)
- Simulation data

© CADFEM Projection Based Model Order Reduction for Multiphysical Problems | Short Course Part 2 – I | Vector Spaces and Subspace Generation 93